High-Voltage, High-Current
OPERATIONAL AMPLIFIER

FEATURES

- ● **WIDE SUPPLY RANGE**
  Single Supply: +8V to +60V
  Dual Supply: ±4V to ±30V
- ● **HIGH OUTPUT CURRENT:**
  3A Continuous
  5A Peak
- ● **WIDE OUTPUT VOLTAGE SWING**
- ● **FULLY PROTECTED:**
  Thermal Shutdown
  Adjustable Current Limit
- ● **OUTPUT DISABLE CONTROL**
- ● **THERMAL SHUTDOWN INDICATOR**
- ● **HIGH SLEW RATE: 10V/μs**
- ● **LOW QUIESCENT CURRENT**
- ● **PACKAGES:**
  7-Lead TO-220, Zip and Straight Leads
  7-Lead DDPAK Surface-Mount

APPLICATIONS

- ● **VALVE, ACTUATOR DRIVERS**
- ● **SYNCHRO, SERVO DRIVERS**
- ● **POWER SUPPLIES**
- ● **TEST EQUIPMENT**
- ● **TRANSDUCER EXCITATION**
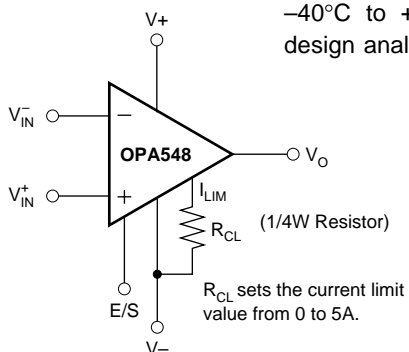- ● **AUDIO AMPLIFIERS**

DESCRIPTION

The OPA548 is a low-cost, high-voltage/high-current operational amplifier ideal for driving a wide variety of loads. A laser-trimmed monolithic integrated circuit provides excellent low-level signal accuracy and high output voltage and current.

The OPA548 operates from either single or dual supplies for design flexibility. In single-supply operation, the input common-mode range extends below ground.

The OPA548 is internally protected against over-temperature conditions and current overloads. In addition, the OPA548 was designed to provide an accurate, user-selected current limit. Unlike other designs which use a "power" resistor in series with the output current path, the OPA548 senses the load indirectly. This allows the current limit to be adjusted from 0A to 5A with a resistor/potentiometer or controlled digitally with a voltage-out or current-out DAC.

The Enable/Status (E/S) pin provides two functions. An input on the pin not only disables the output stage to effectively disconnect the load, but also reduces the quiescent current to conserve power. The E/S pin output can be monitored to determine if the OPA548 is in thermal shutdown.

The OPA548 is available in an industry-standard 7-lead staggered and straight lead TO-220 package, and a 7-lead DDPAK surface-mount plastic power package. The copper tab allows easy mounting to a heat sink or circuit board for excellent thermal performance. It is specified for operation over the extended industrial temperature range, –40°C to +85°C. A SPICE macromodel is available for design analysis.

R_{CL} sets the current limit value from 0 to 5A.

ABSOLUTE MAXIMUM RATINGS[1]

Output Current .... See SOA Curve
Supply Voltage, V+ to V– 60V
Input Voltage .... (V–) – 0.5V to (V+) + 0.5V
Input Shutdown Voltage .... V+
Operating Temperature ....–40°C to +125°C
Storage Temperature ....–55°C to +125°C
Junction Temperature .... 150°C
Lead Temperature (soldering 10s)[2] .... 300°C

NOTES: (1) Stresses above these ratings may cause permanent damage.
(2) Vapor-phase or IR reflow techniques are recommended for soldering the
OPA547F surface-mount package. Wave soldering is not recommended due to
excessive thermal shock and "shadowing" of nearby devices.

⚠ ELECTROSTATIC DISCHARGE SENSITIVITY

This integrated circuit can be damaged by ESD. Texas Instruments recommends that all integrated circuits be handled with appropriate precautions. Failure to observe proper handling and installation procedures can cause damage.

ESD damage can range from subtle performance degradation to complete device failure. Precision integrated circuits may be more susceptible to damage because very small parametric changes could cause the device not to meet its published specifications.

PACKAGE/ORDERING INFORMATION

For the most current package and ordering information, see the Package Ordering Addendum at the end of this data sheet.
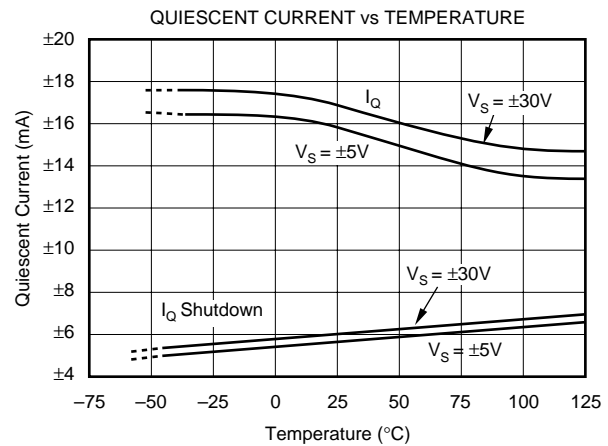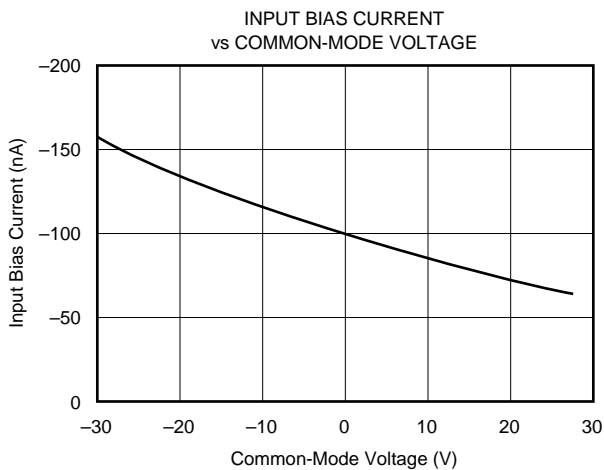
PIN CONFIGURATIONS

NOTE: Tabs are electrically connected to the V– supply.

OPA548
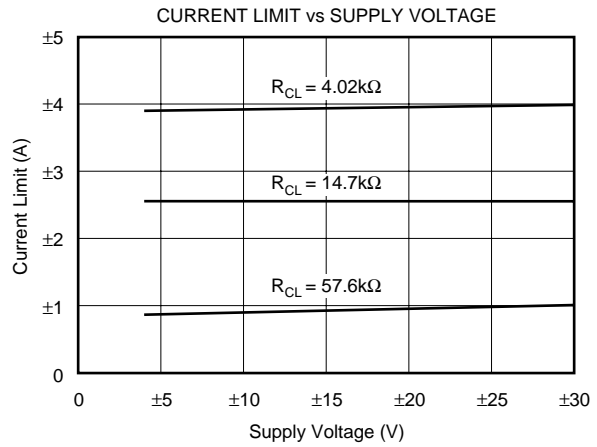SBOS070B
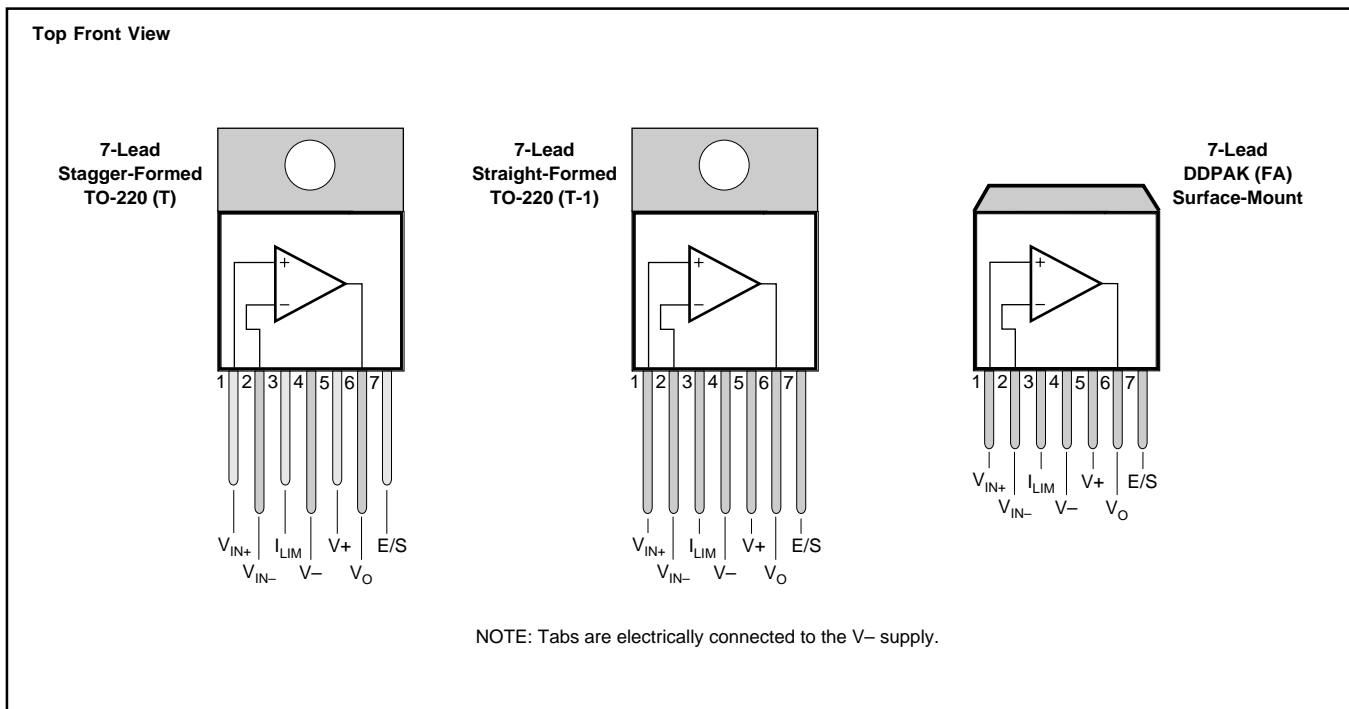
ELECTRICAL CHARACTERISTICS

At T_{CASE} = +25°C, V_S = ±30V and E/S pin open, unless otherwise noted.

PARAMETER	CONDITION	OPA548T, F			UNITS
		MIN	TYP	MAX	
OFFSET VOLTAGE					
Input Offset Voltage	V_{CM} = 0, I_O = 0		±2	±10	mV
vs Temperature	T_A = −40°C to +85°C		±30		µV/°C
vs Power Supply	V_S = ±4V to ±30V		30	100	µV/V
INPUT BIAS CURRENT[1]					
Input Bias Current[2]	V_{CM} = 0V		−100	−500	nA
vs Temperature	T_A = −40°C to +85°C		±0.5		nA/°C
Input Offset Current	V_{CM} = 0V		±5	±50	nA
NOISE					
Input Voltage Noise Density, f = 1kHz			90		nV/$\sqrt{Hz}$
Current Noise Density, f = 1kHz			200		fA/$\sqrt{Hz}$
INPUT VOLTAGE RANGE					
Common-Mode Voltage Range: Positive	Linear Operation	(V+) − 3	(V+) − 2.3		V
Negative	Linear Operation	(V−) − 0.1	(V−) − 0.2		V
Common-Mode Rejection	V_{CM} = (V−) −0.1V to (V+) −3V	80	95		dB
INPUT IMPEDANCE					
Differential			$10^7 \parallel 6$		Ω ‖ pF
Common-Mode			$10^9 \parallel 4$		Ω ‖ pF
OPEN-LOOP GAIN					
Open-Loop Voltage Gain	V_O = ±25V, R_L = 1kΩ	90	98		dB
	V_O = ±25V, R_L = 8Ω		90		dB
FREQUENCY RESPONSE					
Gain-Bandwidth Product	R_L = 8Ω		1		MHz
Slew Rate	G = 1, 50Vp-p, R_L = 8Ω		10		V/µs
Full-Power Bandwidth		See Typical Characteristics			kHz
Settling Time: ±0.1%	G = −10, 50V Step		15		µs
Total Harmonic Distortion + Noise, f = 1kHz	R_L = 8Ω, G = +3, Power = 10W		0.02[3]		%
OUTPUT					
Voltage Output, Positive	I_O = 3A	(V+) − 4.1	(V+) − 3.7		V
Negative	I_O = −3A	(V−) + 3.7	(V−) + 3.3		V
Positive	I_O = 0.6A	(V+) − 2.4	(V+) − 2.1		V
Negative	I_O = −0.6A	(V−) + 1.3	(V−) + 1.0		V
Maximum Continuous Current Output: dc		±3			A
ac		3			Arms
Leakage Current, Output Disabled, dc		See Typical Characteristics			
Output Current Limit					
Current Limit Range			0 to ±5		A
Current Limit Equation		I_{LIM} = (15000)(4.75)/(13750Ω + R_{CL})			A
Current Limit Tolerance[1]	R_{CL} = 14.8kΩ (I_{LIM} = ±2.5A), R_L = 8Ω		±100	±250	mA
Capacitive Load Drive		See Typical Characteristics[4]			
OUTPUT ENABLE /STATUS (E/S) PIN					
Shutdown Input Mode					
$V_{E/S}$ HIGH (output enabled)	E/S Pin Open or Forced High	(V−) + 2.4			V
$V_{E/S}$ LOW (output disabled)	E/S Pin Forced Low			(V−) + 0.8	V
$I_{E/S}$ HIGH (output enabled)	E/S Pin High		−65		µA
$I_{E/S}$ LOW (output disabled)	E/S Pin Low		−70		µA
Output Disable Time			1		µs
Output Enable Time			3		µs
Thermal Shutdown Status Output					
Normal Operation	Sourcing 20µA	(V−) + 2.4	(V−) + 3.5		V
Thermally Shutdown	Sinking 5µA, T_J > 160°C		(V−) + 0.35	(V−) + 0.8	V
Junction Temperature, Shutdown			+160		°C
Reset from Shutdown			+140		°C
POWER SUPPLY					
Specified Voltage			±30		V
Operating Voltage Range		±4		±30	V
Quiescent Current	I_{LIM} Connected to V−, I_O = 0		±17	±20	mA
Quiescent Current, Shutdown Mode	I_{LIM} Connected to V−, I_O = 0		±6		mA
TEMPERATURE RANGE					
Specified Range		−40		+85	°C
Operating Range		−40		+125	°C
Storage Range		−55		+125	°C
Thermal Resistance, θ_{JC}					
7-Lead DDPAK, 7-Lead TO-220	f > 50Hz		2		°C/W
7-Lead DDPAK, 7-Lead TO-220	dc		2.5		°C/W
Thermal Resistance, θ_{JA}					
7-Lead DDPAK, 7-Lead TO-220	No Heat Sink		65		°C/W

NOTES: (1) High-speed test at T_J = +25°C. (2) Positive conventional current flows into the input terminals. (3) See "Total Harmonic Distortion+Noise vs Frequency" in the Typical Characteristics section for additional power levels. (4) See "Small-Signal Overshoot vs Load Capacitance" in the Typical Characteristics section.
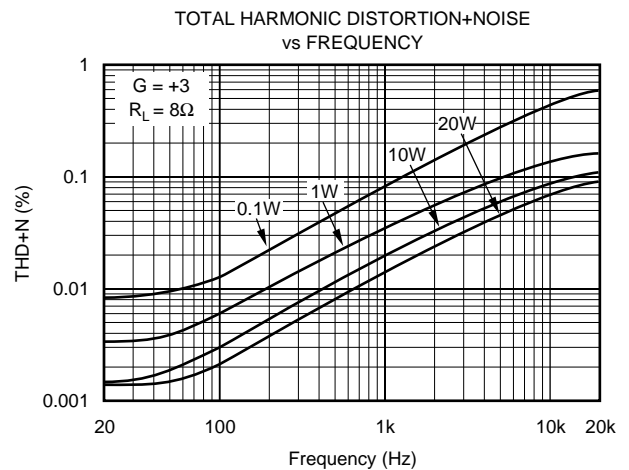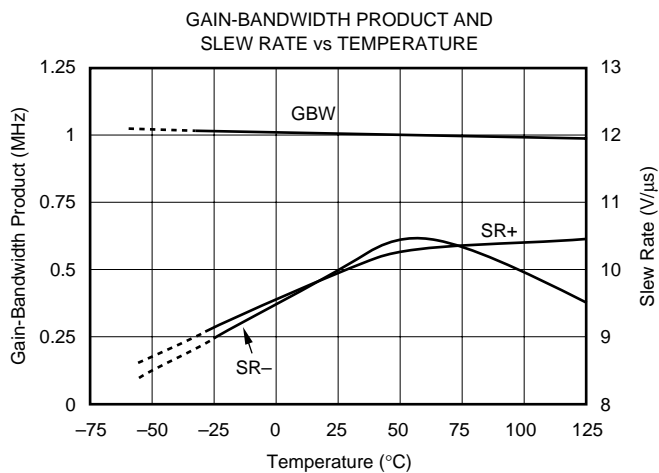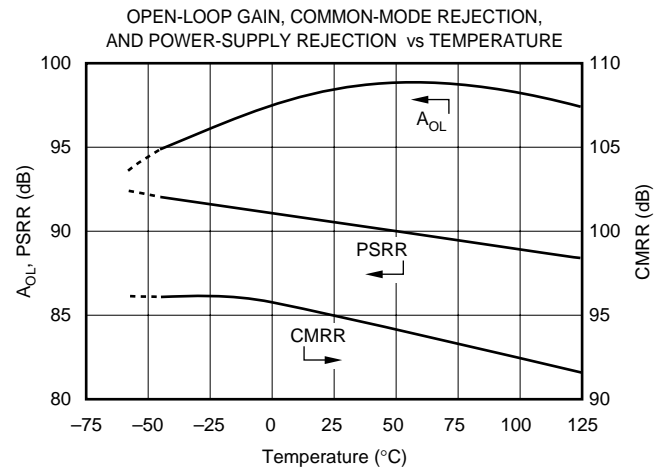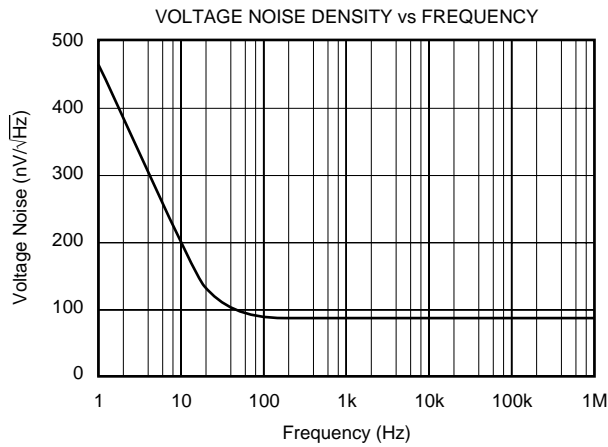
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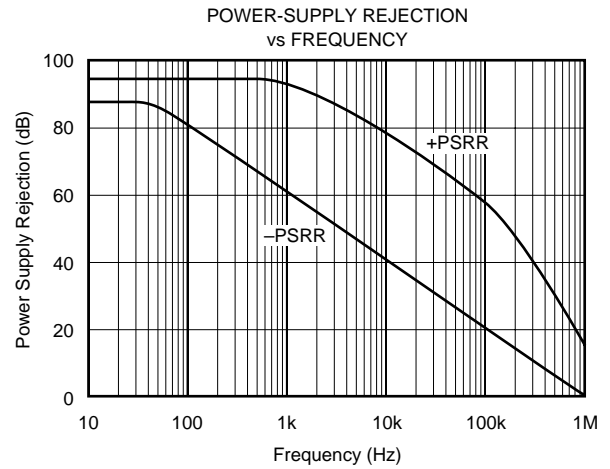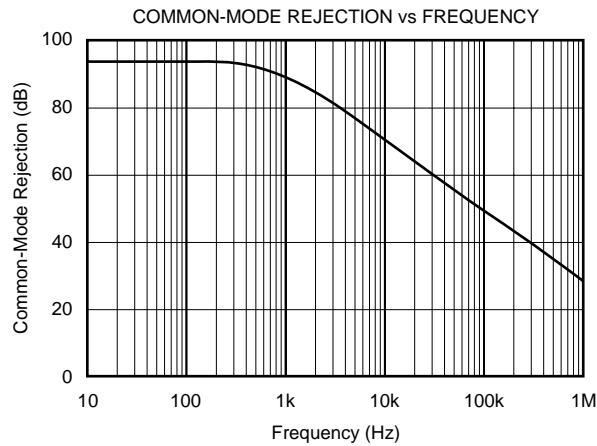# TYPICAL CHARACTERISTICS

At T_{CASE} = +25°C, V_S = ±30V and E/S pin open, unless otherwise noted.

OPEN-LOOP GAIN AND PHASE
vs FREQUENCY

INPUT BIAS CURRENT vs TEMPERATURE

CURRENT LIMIT vs TEMPERATURE

CURRENT LIMIT vs SUPPLY VOLTAGE

INPUT BIAS CURRENT
vs COMMON-MODE VOLTAGE

QUIESCENT CURRENT vs TEMPERATURE

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TYPICAL CHARACTERISTICS (Cont.)

At T_{CASE} = +25°C, V_S = ±30V and E/S pin open, unless otherwise noted.

COMMON-MODE REJECTION vs FREQUENCY

POWER-SUPPLY REJECTION vs FREQUENCY

VOLTAGE NOISE DENSITY vs FREQUENCY

OPEN-LOOP GAIN, COMMON-MODE REJECTION, AND POWER-SUPPLY REJECTION vs TEMPERATURE

GAIN-BANDWIDTH PRODUCT AND SLEW RATE vs TEMPERATURE

TOTAL HARMONIC DISTORTION+NOISE vs FREQUENCY

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TYPICAL CHARACTERISTICS (Cont.)

At T_{CASE} = +25°C, V_S = ±30V and E/S pin open, unless otherwise noted.

OUTPUT VOLTAGE SWING vs OUTPUT CURRENT
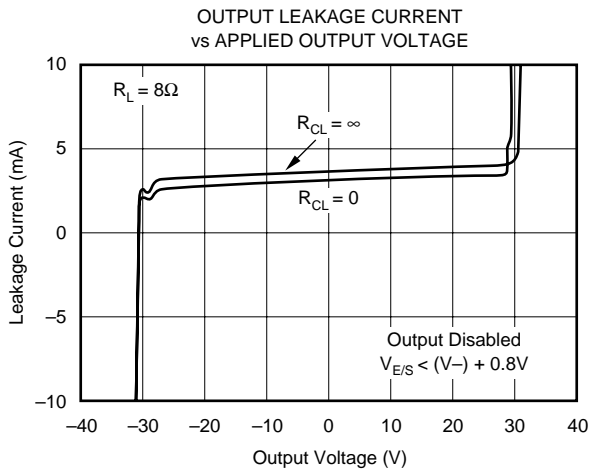
(V+) –V_O

$|(V–) – V_O|$

OUTPUT VOLTAGE SWING vs TEMPERATURE

I_O = +3A

I_O = –3A

I_O = +0.6A

I_O = –0.6A

MAXIMUM OUTPUT VOLTAGE SWING vs FREQUENCY

Maximum Output Voltage Without Slew Rate Induced Distortion

OUTPUT LEAKAGE CURRENT vs APPLIED OUTPUT VOLTAGE

R_L = 8Ω

R_{CL} = ∞

R_{CL} = 0

Output Disabled
$V_{E/S}$ < (V–) + 0.8V

OFFSET VOLTAGE PRODUCTION DISTRIBUTION

Typical distribution of packaged units.

OFFSET VOLTAGE DRIFT PRODUCTION DISTRIBUTION

Typical production distribution of packaged units.

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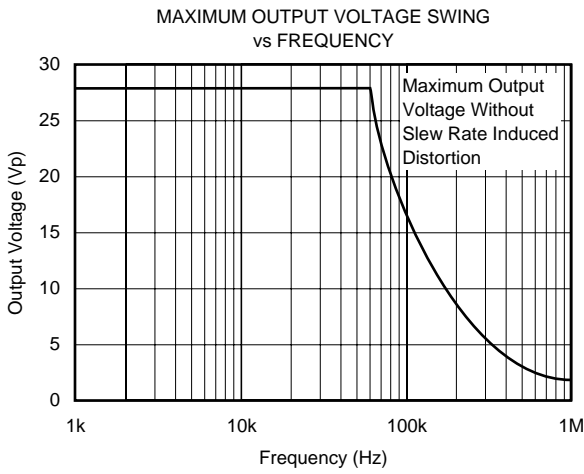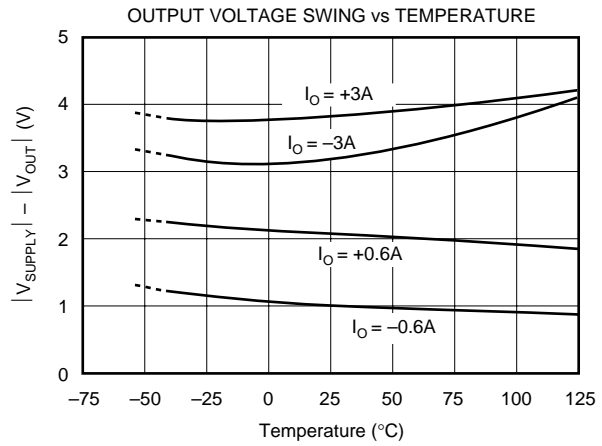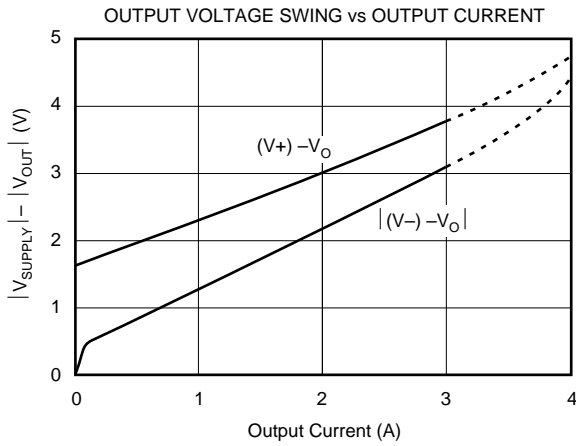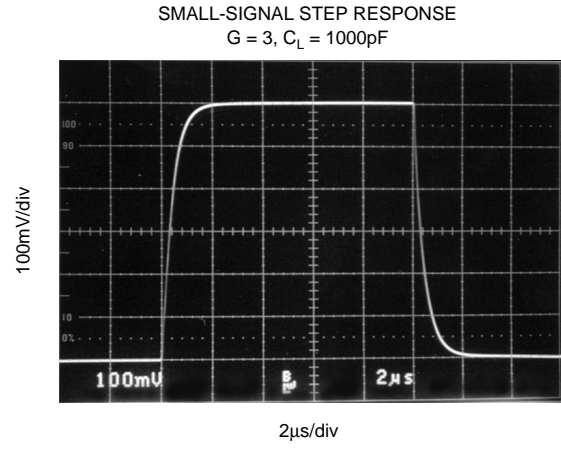# TYPICAL CHARACTERISTICS (Cont.)

At T_{CASE} = +25°C, V_S = ±30V and E/S pin open, unless otherwise noted.

SMALL-SIGNAL OVERSHOOT
vs LOAD CAPACITANCE

LARGE-SIGNAL STEP RESPONSE
G = 3, C_L = 1000pF, R_L = 8Ω

5µs/div

SMALL-SIGNAL STEP RESPONSE
G = 1, C_L = 1000pF

2µs/div

SMALL-SIGNAL STEP RESPONSE
G = 3, C_L = 1000pF

2µs/div

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APPLICATIONS INFORMATION

Figure 1 shows the OPA548 connected as a basic noninverting amplifier. The OPA548 can be used in virtually any op amp configuration.

Power-supply terminals should be bypassed with low series impedance capacitors. The technique shown in Figure 7, using a ceramic and tantalum type in parallel is recommended. In addition, we recommend a 0.01µF capacitor between V+ and V− as close to the OPA548 as possible. Power-supply wiring should have low series impedance.
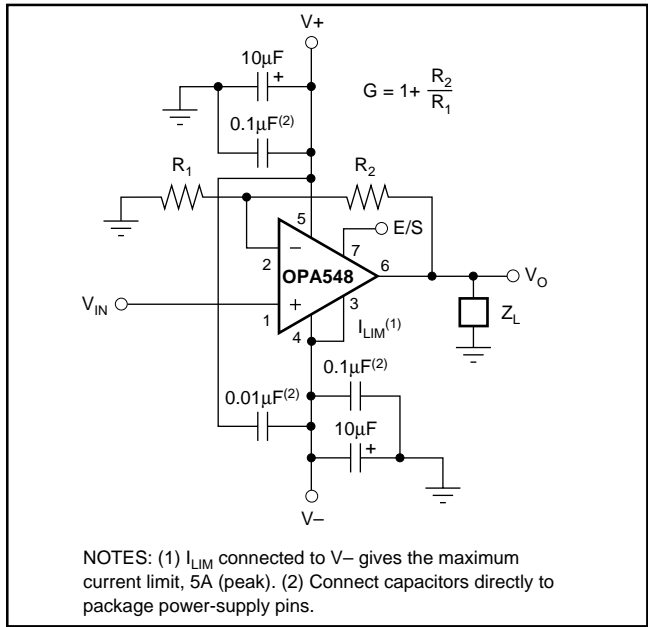

NOTES: (1) I_{LIM} connected to V− gives the maximum current limit, 5A (peak). (2) Connect capacitors directly to package power-supply pins.

FIGURE 1. Basic Circuit Connections.

POWER SUPPLIES

The OPA548 operates from single (+8V to +60V) or dual (±4V to ±30V) supplies with excellent performance. Most behavior remains unchanged throughout the full operating voltage range. Parameters which vary significantly with operating voltage are shown in the typical characteristic curves.

Some applications do not require equal positive and negative output voltage swing. Power-supply voltages do not need to be equal. The OPA548 can operate with as little as 8V between the supplies and with up to 60V between the supplies. For example, the positive supply could be set to 55V with the negative supply at –5V, or vice-versa.

ADJUSTABLE CURRENT LIMIT

The OPA548 features an accurate, user-selected current limit. Current limit is set from 0A to 5A by controlling the input to the I_{LIM} pin. Unlike other designs which use a power resistor in series with the output current path, the OPA548 senses the load indirectly. This allows the current limit to be set with a 0µA to 330µA control signal. In contrast, other designs require a limiting resistor to handle the full output current (5A in this case).

With the OPA548, the simplest method for adjusting the current limit uses a resistor or potentiometer connected between the I_{LIM} pin and V− according to the Equation 1:

$$R_{CL} = \frac{(15000)(4.75)}{I_{LIM}} - 13750\Omega \qquad (1)$$

The low-level control signal (0µA to 330µA) also allows the current limit to be digitally controlled.

See Figure 3 for a simplified schematic of the internal circuitry used to set the current limit. Leaving the I_{LIM} pin open programs the output current to zero, while connecting I_{LIM} directly to V− programs the maximum output current limit, typically 5A.

SAFE OPERATING AREA

Stress on the output transistors is determined both by the output current and by the output voltage across the conducting output transistor, $V_S - V_O$. The power dissipated by the output transistor is equal to the product of the output current and the voltage across the conducting transistor, $V_S - V_O$. The Safe Operating Area (SOA curve, Figure 2) shows the permissible range of voltage and current.
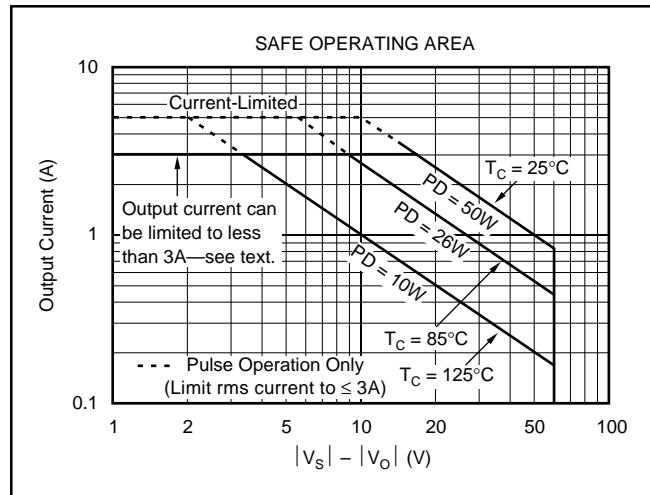
FIGURE 2. Safe Operating Area.

The safe output current decreases as $V_S - V_O$ increases. Output short-circuits are a very demanding case for SOA. A short-circuit to ground forces the full power-supply voltage (V+ or V−) across the conducting transistor. Increasing the case temperature reduces the safe output current that can be tolerated without activating the thermal shutdown circuit of the OPA548. For further insight on SOA, consult Application Bulletin SBOA022.

AMPLIFIER MOUNTING

Figure 4 provides recommended solder footprints for both the TO-220 and DDPAK power packages. The tab of both packages is electrically connected to the negative supply, V−. It may be desirable to isolate the tab of the TO-220 package from its

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FIGURE 3. Adjustable Current Limit.

RESISTOR METHOD
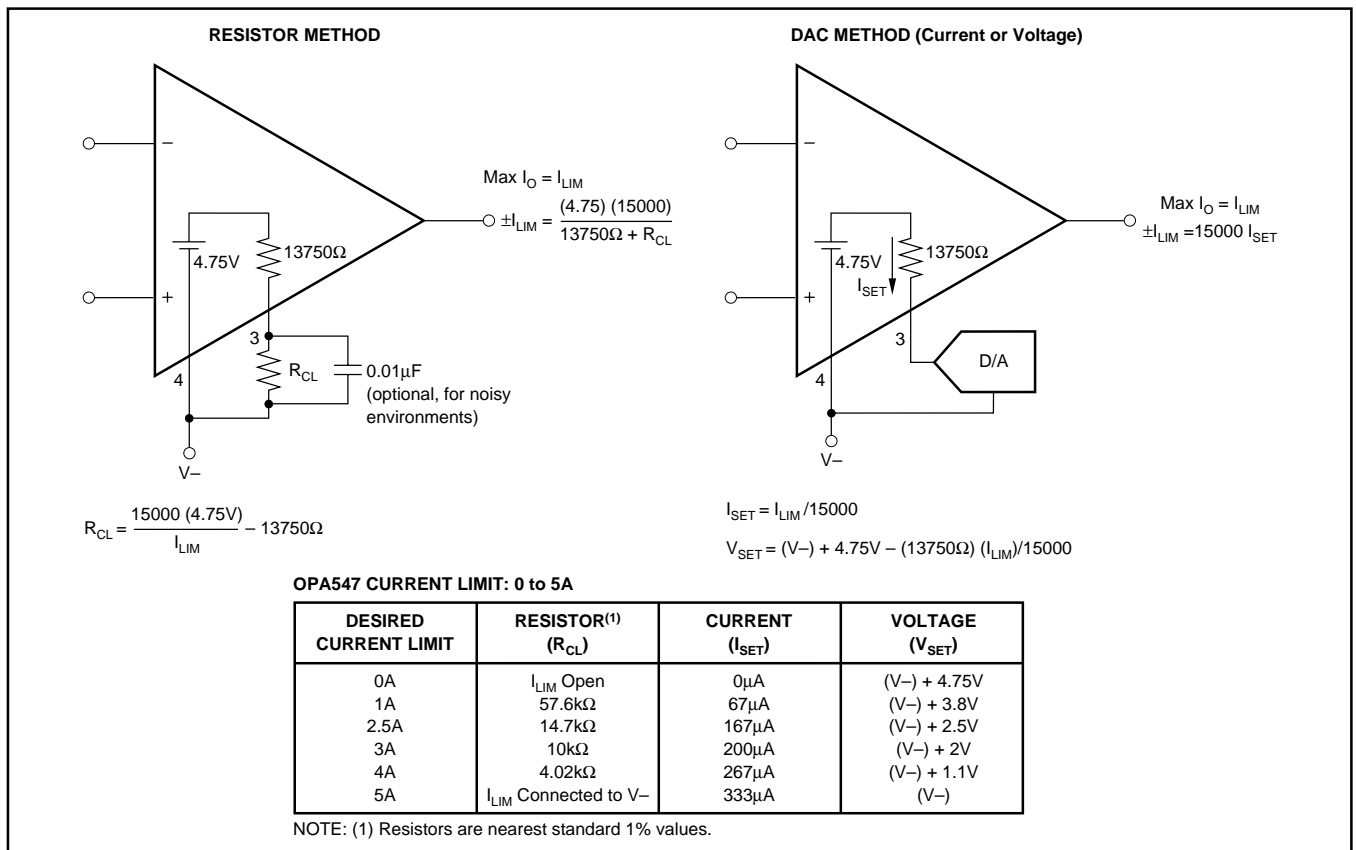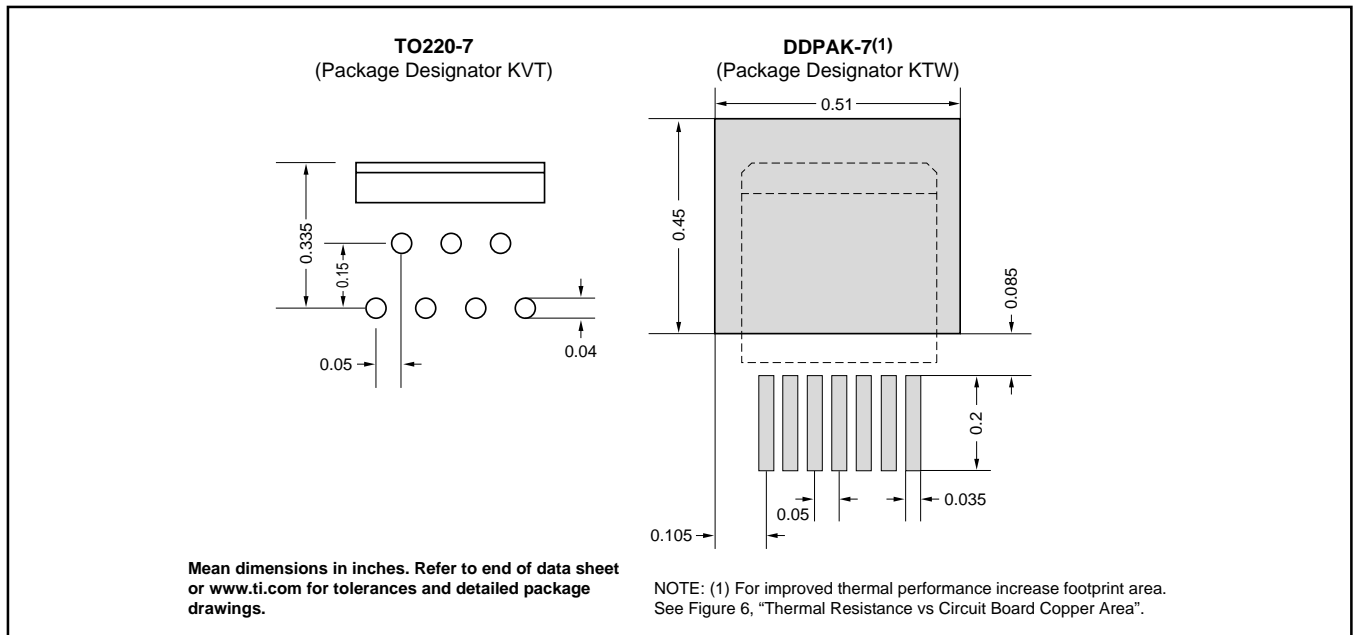
Max $I_O = I_{LIM}$

$$\pm I_{LIM} = \frac{(4.75)\,(15000)}{13750\Omega + R_{CL}}$$

$$R_{CL} = \frac{15000\,(4.75V)}{I_{LIM}} - 13750\Omega$$

DAC METHOD (Current or Voltage)

Max $I_O = I_{LIM}$

$\pm I_{LIM} = 15000\,I_{SET}$

$I_{SET} = I_{LIM}/15000$

$V_{SET} = (V-) + 4.75V - (13750\Omega)\,(I_{LIM})/15000$

OPA547 CURRENT LIMIT: 0 to 5A

DESIRED CURRENT LIMIT	RESISTOR[1] (R_{CL})	CURRENT (I_{SET})	VOLTAGE (V_{SET})
0A	I_{LIM} Open	0μA	(V–) + 4.75V
1A	57.6kΩ	67μA	(V–) + 3.8V
2.5A	14.7kΩ	167μA	(V–) + 2.5V
3A	10kΩ	200μA	(V–) + 2V
4A	4.02kΩ	267μA	(V–) + 1.1V
5A	I_{LIM} Connected to V–	333μA	(V–)

NOTE: (1) Resistors are nearest standard 1% values.

FIGURE 4. TO-220 and DDPAK Solder Footprints.

TO220-7
(Package Designator KVT)

Mean dimensions in inches. Refer to end of data sheet or www.ti.com for tolerances and detailed package drawings.

DDPAK-7[1]
(Package Designator KTW)

NOTE: (1) For improved thermal performance increase footprint area. See Figure 6, "Thermal Resistance vs Circuit Board Copper Area".

mounting surface with a mica (or other film) insulator (see Figure 5). For lowest overall thermal resistance it is best to isolate the entire heat sink/OPA548 structure from the mounting surface rather than to use an insulator between the semiconductor and heat sink.

For best thermal performance, the tab of the DDPAK surface-mount version should be soldered directly to a circuit board copper area. Increasing the copper area improves

heat dissipation. See Figure 6 for typical thermal resistance from junction-to-ambient as a function of the copper area.

POWER DISSIPATION

Power dissipation depends on power supply, signal, and load conditions. For dc signals, power dissipation is equal to the product of output current times the voltage across the
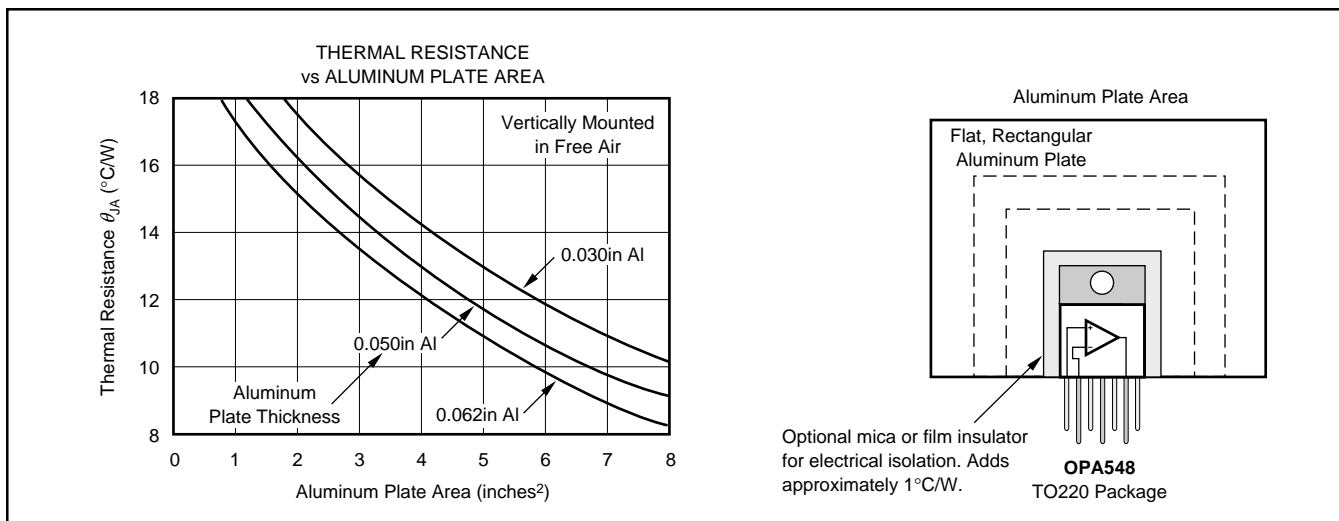
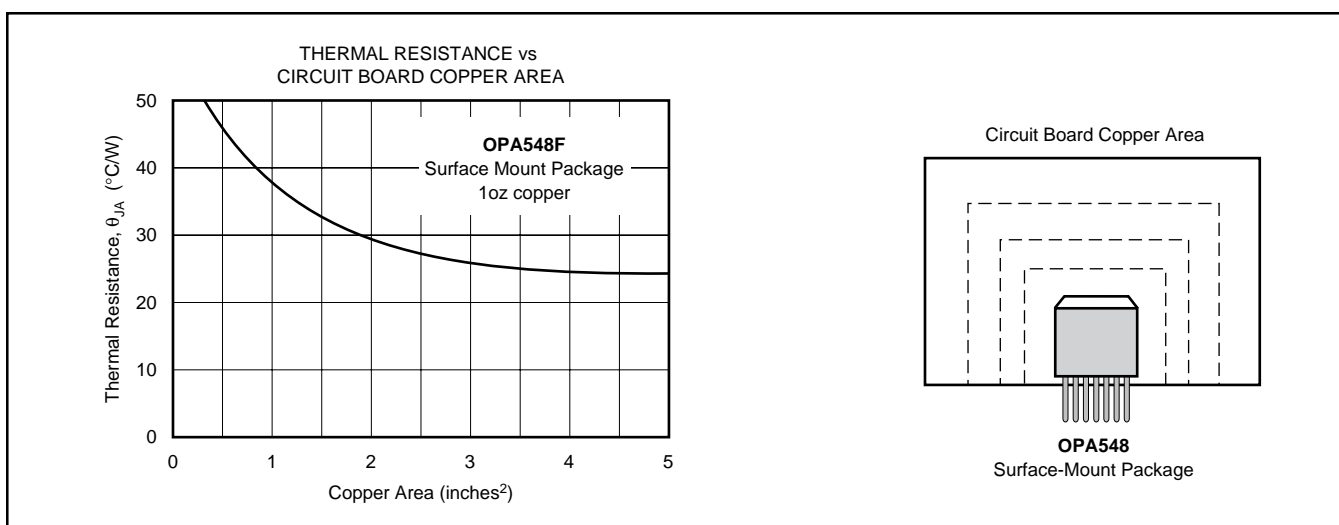FIGURE 5. TO-220 Thermal Resistance vs Aluminum Plate Area.

FIGURE 6. DDPAK Thermal Resistance vs Circuit Board Copper Area.

conducting output transistor. Power dissipation can be minimized by using the lowest possible power-supply voltage necessary to assure the required output voltage swing.

For resistive loads, the maximum power dissipation occurs at a dc output voltage of one-half the power-supply voltage. Dissipation with ac signals is lower. Application Bulletin SBOA022 explains how to calculate or measure power dissipation with unusual signals and loads.

THERMAL PROTECTION

Power dissipated in the OPA548 will cause the junction temperature to rise. The OPA548 has thermal shutdown circuitry that protects the amplifier from damage. The thermal protection circuitry disables the output when the junction temperature reaches approximately 160°C, allowing the device to cool. When the junction temperature cools to approximately 140°C, the output circuitry is again enabled. Depending on load and signal conditions, the thermal protection circuit may cycle on and off. This limits the dissipation of the amplifier but may have an undesirable effect on the load.

Any tendency to activate the thermal protection circuit indicates excessive power dissipation or an inadequate heat sink. For reliable operation, junction temperature should be limited to 125°C, maximum. To estimate the margin of safety in a complete design (including heat sink) increase the ambient temperature until the thermal protection is triggered. Use worst-case load and signal conditions. For good reliability, thermal protection should trigger more than 35°C above the maximum expected ambient condition of your application. This produces a junction temperature of 125°C at the maximum expected ambient condition.

The internal protection circuitry of the OPA548 was designed to protect against overload conditions. It was not intended to replace proper heat sinking. Continuously running the OPA548 into thermal shutdown will degrade reliability.

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HEAT SINKING

Most applications require a heat sink to assure that the maximum operating junction temperature (125°C) is not exceeded. In addition, the junction temperature should be kept as low as possible for increased reliability. Junction temperature can be determined according to the equation:

$$T_J = T_A + P_D\theta_{JA} \tag{1}$$

$$\text{where, } \theta_{JA} = \theta_{JC} + \theta_{CH} + \theta_{HA} \tag{2}$$

T_J = Junction Temperature (°C)
T_A = Ambient Temperature (°C)
P_D = Power Dissipated (W)
θ_{JC} = Junction-to-Case Thermal Resistance (°C/W)
θ_{CH} = Case-to-Heat Sink Thermal Resistance (°C/W)
θ_{HA} = Heat Sink-to-Ambient Thermal Resistance (°C/W)
θ_{JA} = Junction-to-Air Thermal Resistance (°C/W)

Figure 7 shows maximum power dissipation versus ambient temperature with and without the use of a heat sink. Using a heat sink significantly increases the maximum power dissipation at a given ambient temperature as shown.

The difficulty in selecting the heat sink required lies in determining the power dissipated by the OPA548. For dc output into a purely resistive load, power dissipation is simply the load current times the voltage developed across the conducting output transistor, $P_D = I_L(V_S–V_O)$. Other loads are not as simple. Consult Application Bulletin SBOA022 for further insight on calculating power dissipation. Once power dissipation for an application is known, the proper heat sink can be selected.
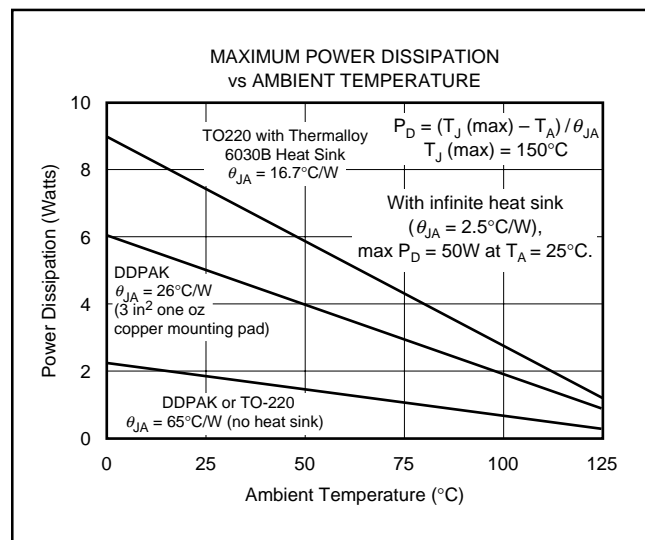

FIGURE 7. Maximum Power Dissipation vs Ambient Temperature.

Heat Sink Selection Example

A TO-220 package is dissipating 5W. The maximum expected ambient temperature is 40°C. Find the proper heat sink to keep the junction temperature below 125°C (150°C minus 25°C safety margin).

Combining equations (1) and (2) gives:

$$T_J = T_A + P_D(\theta_{JC} + \theta_{CH} + \theta_{HA}) \tag{3}$$

T_J, T_A, and P_D are given. θ_{JC} is provided in the specification table, 2.5°C/W (dc). θ_{CH} can be obtained from the heat sink manufacturer. Its value depends on heat sink size, area, and material used. Semiconductor package type, mounting screw torque, insulating material used (if any), and thermal joint compound used (if any) also affect θ_{CH}. A typical θ_{CH} for a TO-220 mounted package is 1°C/W. Now we can solve for θ_{HA}:

$$\theta_{HA} = \frac{T_J - T_A}{P_D} - (\theta_{JC} + \theta_{CH})$$

$$\theta_{HA} = \frac{125°C - 40°C}{5W} - (2.5°C/W + 1°C/W) = 13.5°C/W$$

To maintain junction temperature below 125°C, the heat sink selected must have a θ_{HA} less than 14°C/W. In other words, the heat sink temperature rise above ambient must be less than 67.5°C (13.5°C/W • 5W). For example, at 5W Thermalloy model number 6030B has a heat sink temperature rise of 66°C above ambient (θ_{HA} = 66°C/5W = 13.2°C/W), which is below the 67.5°C required in this example. Figure 7 shows power dissipation versus ambient temperature for a TO-220 package with a 6030B heat sink.

Another variable to consider is natural convection versus forced convection air flow. Forced-air cooling by a small fan can lower θ_{CA} ($\theta_{CH} + \theta_{HA}$) dramatically. Heat sink manufactures provide thermal data for both of these cases. For additional information on determining heat sink requirements, consult Application Bulletin SBOA021.

As mentioned earlier, once a heat sink has been selected, the complete design should be tested under worst-case load and signal conditions to ensure proper thermal protection.

ENABLE/STATUS (E/S) PIN

The Enable/Status pin provides two functions: forcing this pin LOW disables the output stage, or E/S can be monitored to determine if the OPA548 is in thermal shutdown. One or both of these functions can be utilized on the same device using single or dual supplies. For normal operation (output enabled), the E/S pin can be left open or pulled HIGH (at least 2.4V above the negative rail). A small value capacitor connected between the E/S pin and V– may be required for noisy applications.

Output Disable

A unique feature of the OPA548 is its output disable capability. This function not only conserves power during idle periods (quiescent current drops to approximately 6mA), but also allows multiplexing in low frequency (f < 20kHz), multichannel applications. Signals greater than 20kHz may cause leakage current to increase in devices that are shutdown. Figure 18 shows the two OPA548s in a switched amplifier configuration. The on/off state of the two amplifiers is controlled by the voltage on the E/S pin.

To disable the output, the E/S pin is pulled LOW, no greater than 0.8V above the negative rail. Typically the output is shutdown in 1µs. Figure 8 provides an example of how to implement this function using a single supply. Figure 9 gives a circuit for dual-supply applications. To return the output to an enabled state, the E/S pin should be disconnected (open) or pulled to at least (V–) + 2.4V. It should be noted that pulling the E/S pin HIGH (output enabled) does not disable internal thermal shutdown.
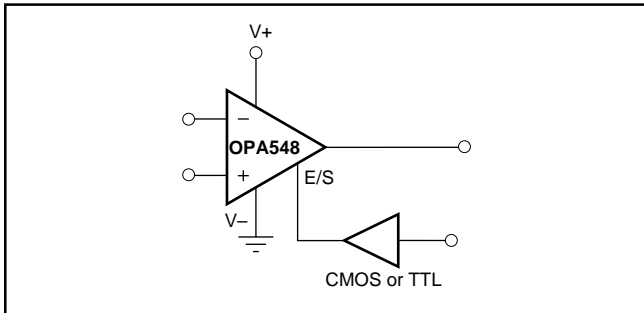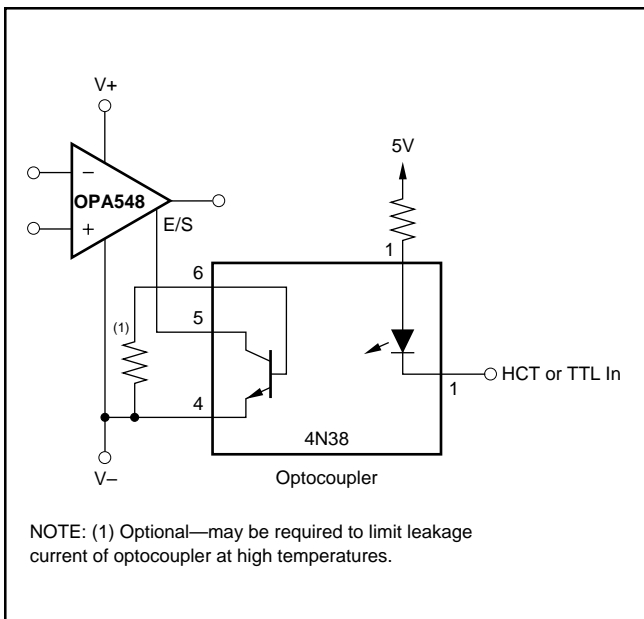

FIGURE 8. Output Disable with a Single Supply.

NOTE: (1) Optional—may be required to limit leakage current of optocoupler at high temperatures.

FIGURE 9. Output Disable with Dual Supplies.

Thermal Shutdown Status

Internal thermal shutdown circuitry shuts down the output when the die temperature reaches approximately 160°C, resetting when the die has cooled to 140°C. The E/S pin can be monitored to determine if shutdown has occurred. During normal operation the voltage on the E/S pin is typically 3.5V above the negative rail. Once shutdown has occurred, this voltage drops to approximately 350mV above the negative rail.

Figure 10 gives an example of monitoring shutdown in a single-supply application. Figure 11 provides a circuit for dual supplies. External logic circuitry or an LED could be used to indicate if the output has been thermally shutdown, see Figure 16.
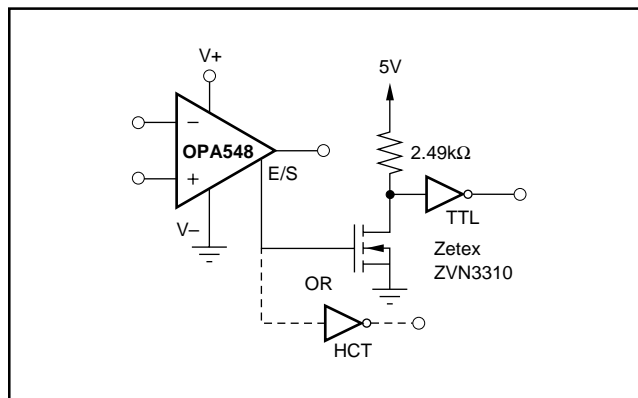

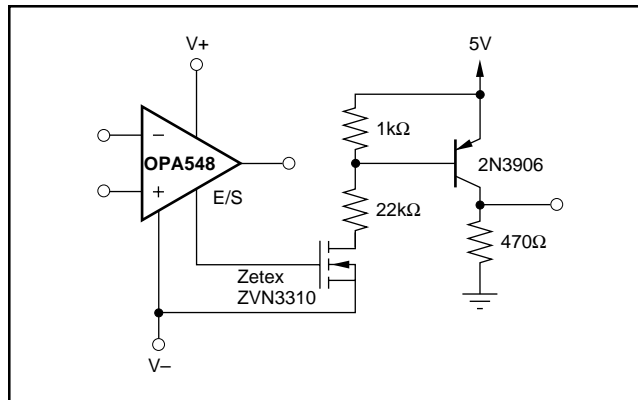FIGURE 10. Thermal Shutdown Status with a Single Supply.

FIGURE 11. Thermal Shutdown Status with Dual Supplies.

Output Disable and Thermal Shutdown Status

As mentioned earlier, the OPA548's output can be disabled and the disable status can be monitored simultaneously. Figures 12 and 13 provide examples interfacing to the E/S pin while using a single supply and dual supplies, respectively.

OUTPUT STAGE COMPENSATION

The complex load impedances common in power op amp applications can cause output stage instability. For normal operation output compensation circuitry is typically not required. However, if the OPA548 is intended to be driven into current limit, an R/C network may be required. See Figure 14 for an output series R/C compensation (snubber) network which generally provides excellent stability.

A snubber circuit may also enhance stability when driving large capacitive loads (> 1000pF) or inductive loads (motors, loads separated from the amplifier by long cables). Typically 3Ω to 10Ω in series with 0.01µF to 0.1µF is adequate. Some variations in circuit value may be required with certain loads.

OUTPUT PROTECTION

Reactive and EMF-generating loads can return load current to the amplifier, causing the output voltage to exceed the power-supply voltage. This damaging condition can be
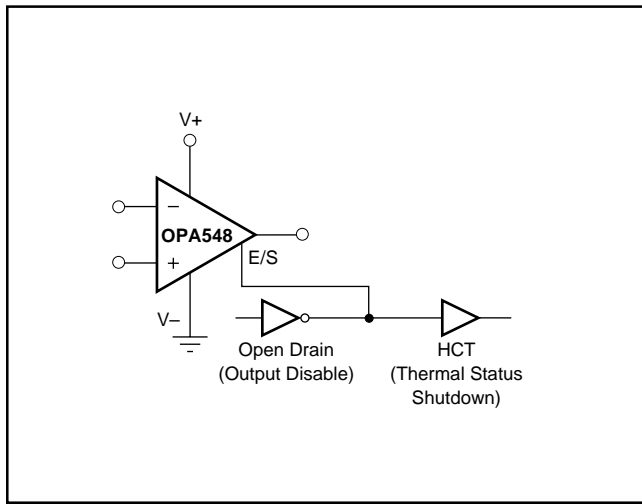
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FIGURE 12. Output Disable and Thermal Shutdown Status with a Single Supply.

$$G = -\frac{R_2}{R_1} = -4$$

D_1, D_2 : Motorola MUR410.

FIGURE 14. Motor Drive Circuit.

NOTE: (1) Optional—may be required to limit leakage current of optocoupler at high temperatures.
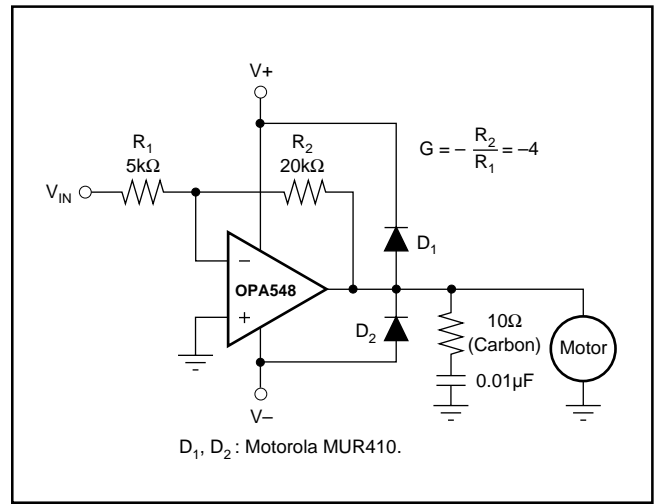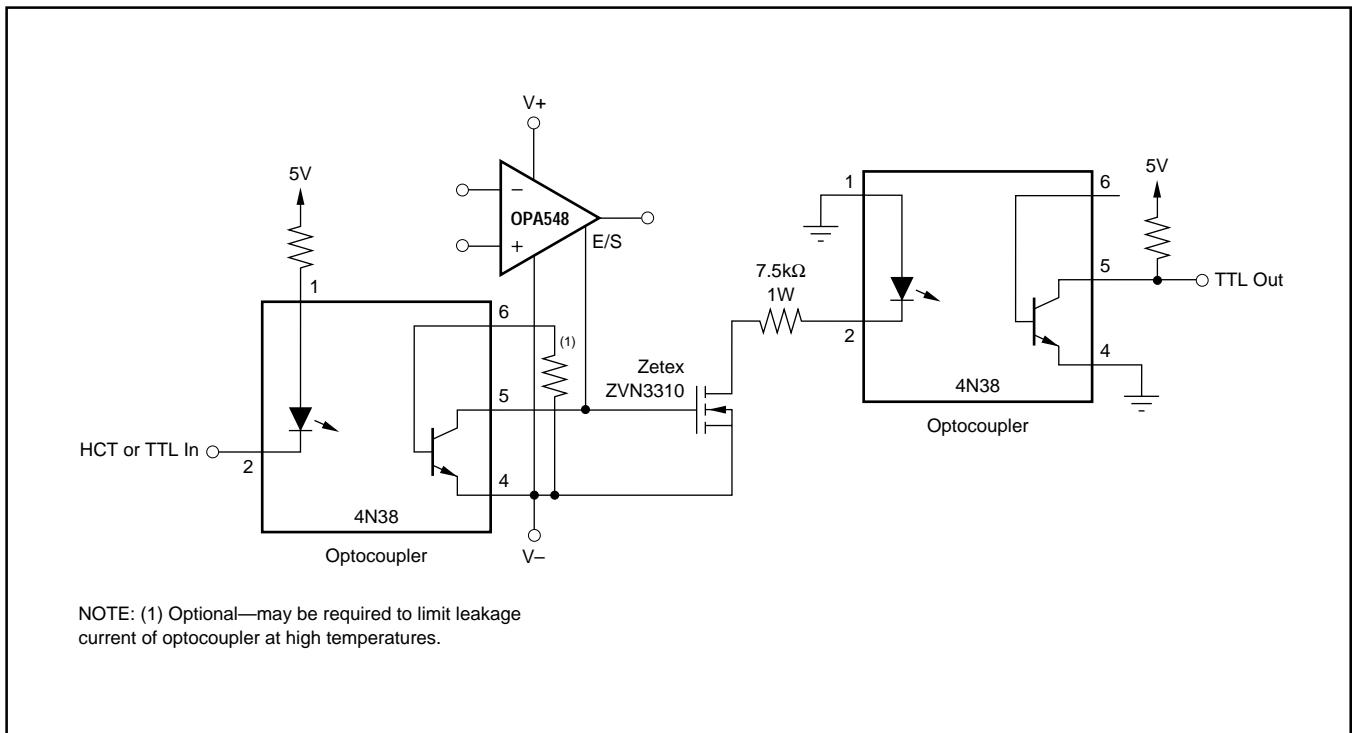
FIGURE 13. Output Disable and Thermal Shutdown Status with Dual Supplies.

avoided with clamp diodes from the output terminal to the power supplies, as shown in Figure 14. Schottky rectifier diodes with a 5A or greater continuous rating are recommended.

VOLTAGE SOURCE APPLICATION

Figure 15 illustrates how to use the OPA548 to provide an accurate voltage source with only three external resistors. First, the current limit resistor, R_{CL}, is chosen according to the desired output current. The resulting voltage at the I_{LIM} pin is constant and stable over temperature. This voltage, V_{CL}, is connected to the noninverting input of the op amp and

used as a voltage reference, thus eliminating the need for an external reference. The feedback resistors are selected to gain V_{CL} to the desired output voltage level.

PROGRAMMABLE POWER SUPPLY

A programmable source/sink power supply can easily be built using the OPA548. Both the output voltage and output current are user-controlled. See Figure 16 for a circuit using potentiometers to adjust the output voltage and current while Figure 17 uses DACs. An LED tied to the E/S pin through a logic gate indicates if the OPA548 is in thermal shutdown.

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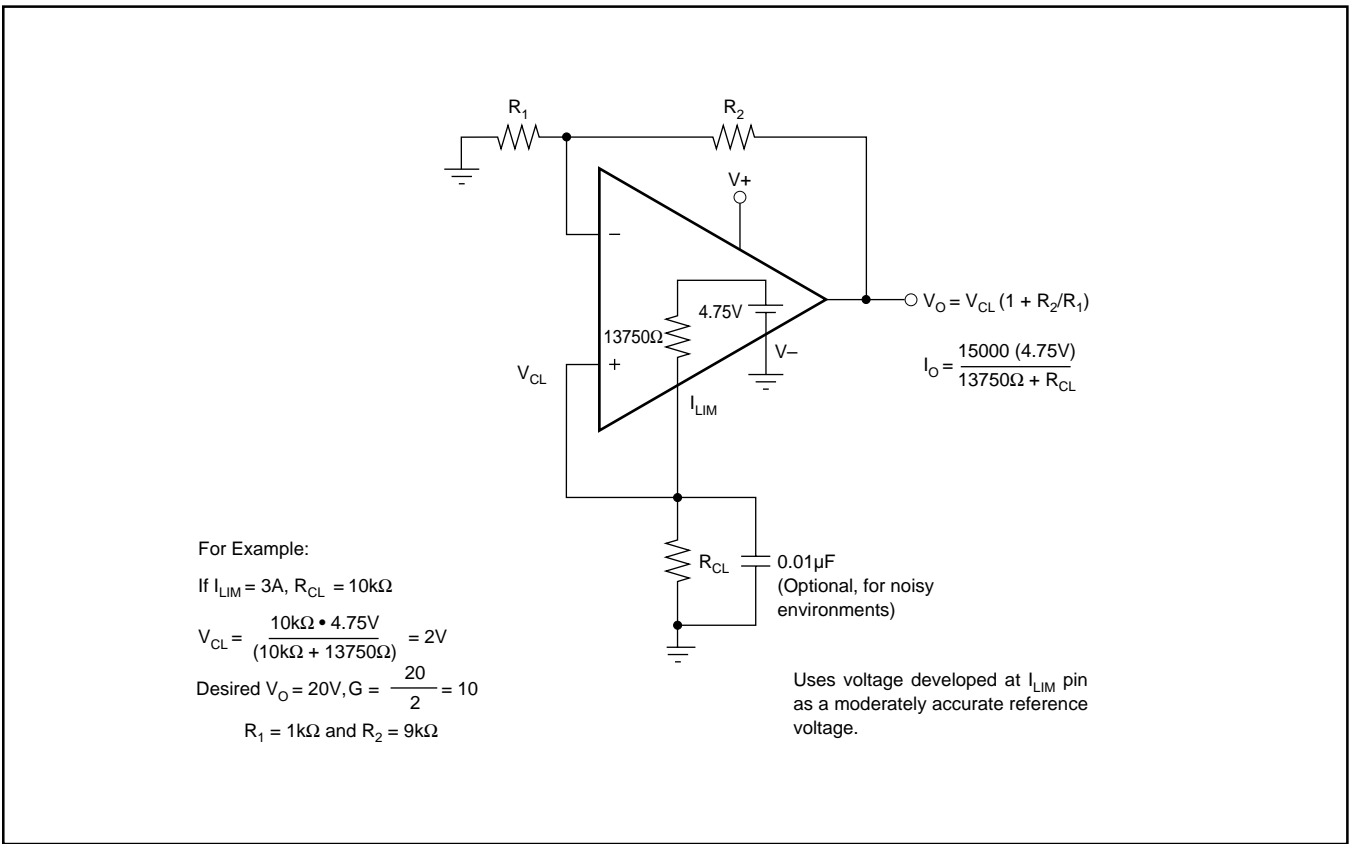
FIGURE 15. Voltage Source.

$V_O = V_{CL}(1 + R_2/R_1)$

$$I_O = \frac{15000 \, (4.75V)}{13750\Omega + R_{CL}}$$

4.75V

13750Ω

V_{CL}

I_{LIM}

R_{CL}

0.01µF
(Optional, for noisy environments)

For Example:

If $I_{LIM} = 3A$, $R_{CL} = 10k\Omega$

$$V_{CL} = \frac{10k\Omega \cdot 4.75V}{(10k\Omega + 13750\Omega)} = 2V$$

Desired $V_O = 20V$, $G = \dfrac{20}{2} = 10$

$R_1 = 1k\Omega$ and $R_2 = 9k\Omega$

Uses voltage developed at I_{LIM} pin as a moderately accurate reference voltage.
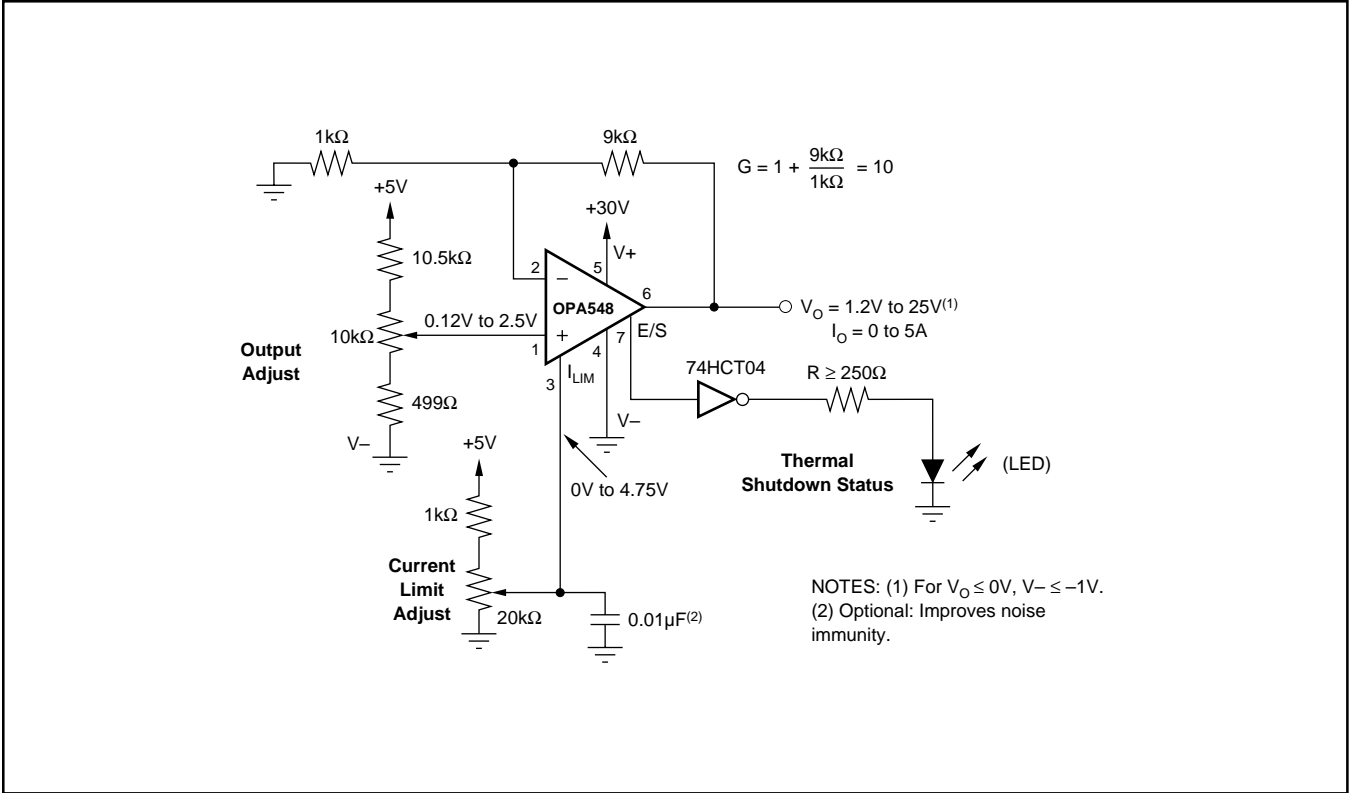
FIGURE 16. Resistor-Controlled Programmable Power Supply.

$$G = 1 + \frac{9k\Omega}{1k\Omega} = 10$$

1kΩ

9kΩ

+5V

10.5kΩ

10kΩ

0.12V to 2.5V

499Ω

Output Adjust

V−

+30V

V+

OPA548

E/S

I_{LIM}

V−

0V to 4.75V

$V_O = 1.2V$ to $25V^{(1)}$

$I_O = 0$ to 5A

74HCT04

$R \geq 250\Omega$

(LED)

Thermal Shutdown Status

+5V

1kΩ

Current Limit Adjust

20kΩ

0.01µF$^{(2)}$

NOTES: (1) For $V_O \leq 0V$, $V- \leq -1V$.
(2) Optional: Improves noise immunity.

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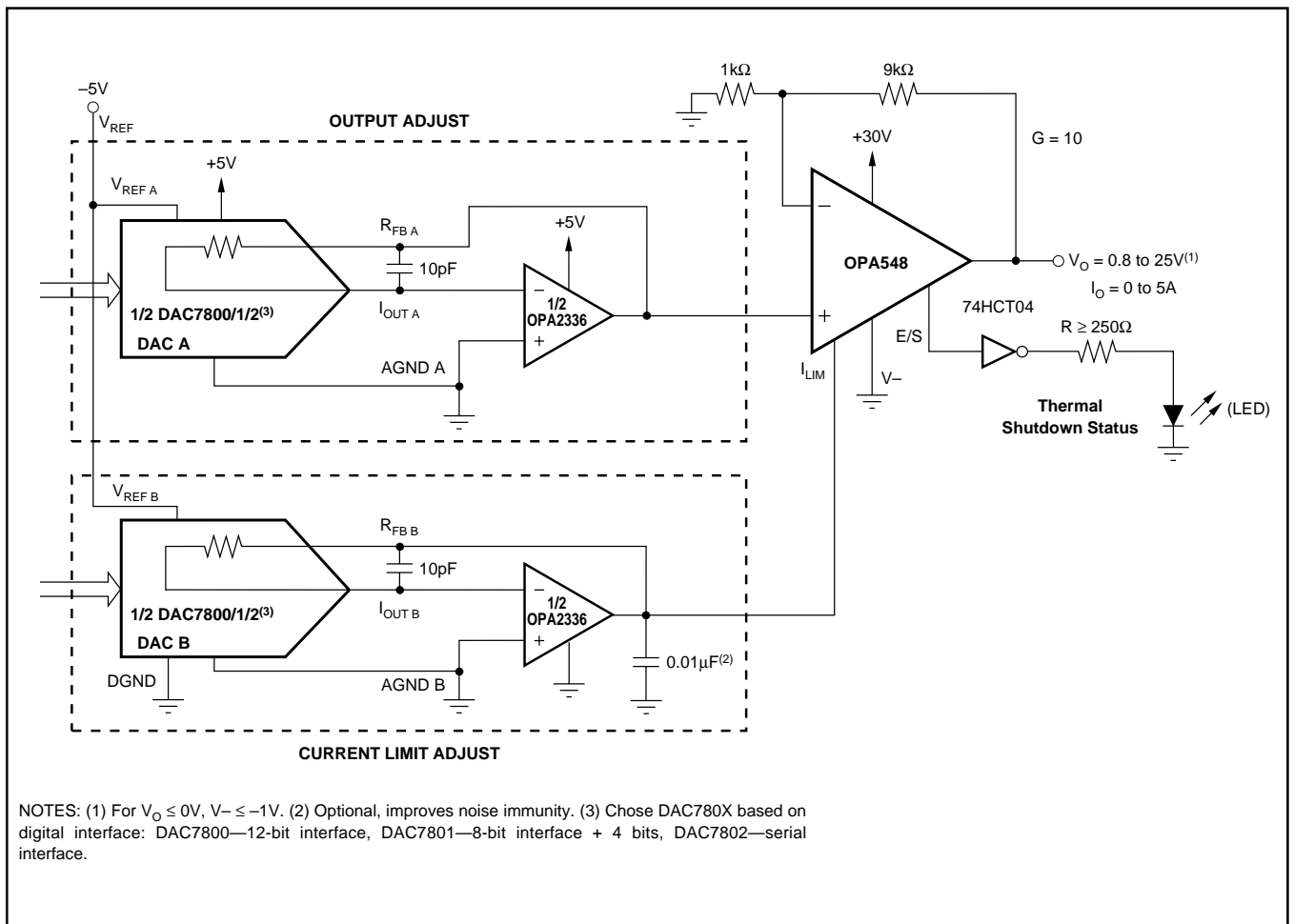
FIGURE 17. Digitally-Controlled Programmable Power Supply.

NOTES: (1) For $V_O \leq 0V$, $V- \leq -1V$. (2) Optional, improves noise immunity. (3) Chose DAC780X based on digital interface: DAC7800—12-bit interface, DAC7801—8-bit interface + 4 bits, DAC7802—serial interface.

$V_{E/S} > (V-) +2.4V$: Amp 1 is on, Amp 2 if off

$\longrightarrow V_O = -V_{IN1}\left(\dfrac{R_2}{R_1}\right)$

$V_{E/S} < (V-) +2.4V$: Amp 2 is on, Amp 1 if off

$\longrightarrow V_O = -V_{IN2}\left(\dfrac{R_4}{R_3}\right)$
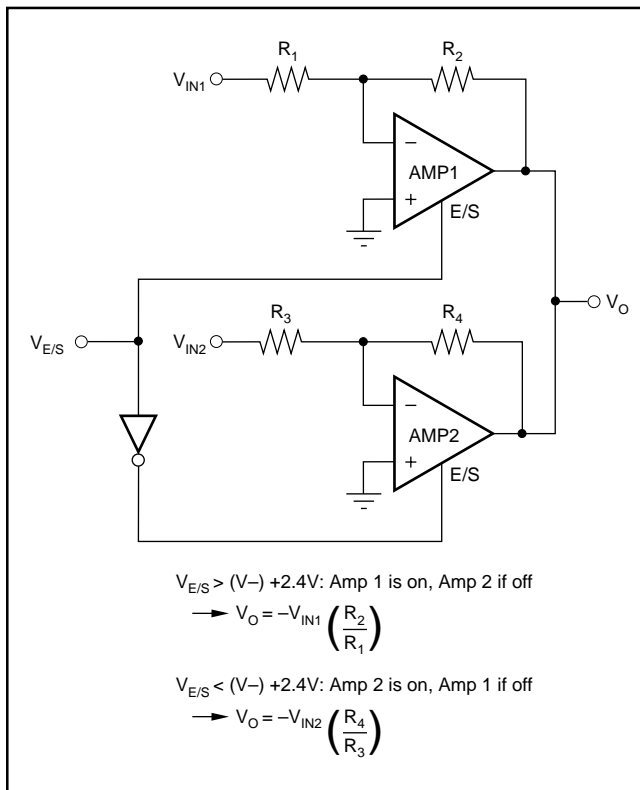
FIGURE 18. Switched Amplifier.
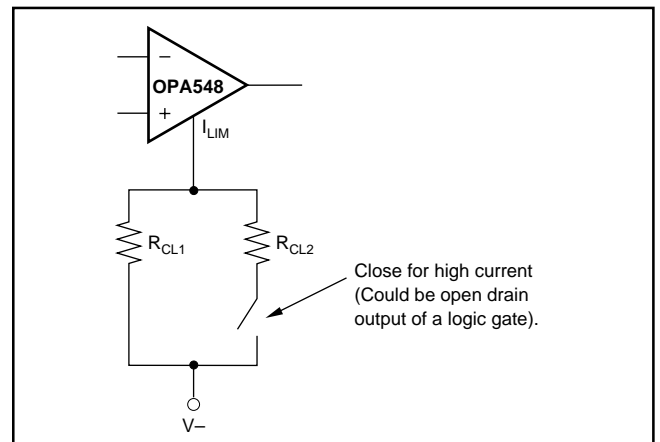
FIGURE 19. Multiple Current Limit Values.

As V_O increases, I_{LIM} decreases.
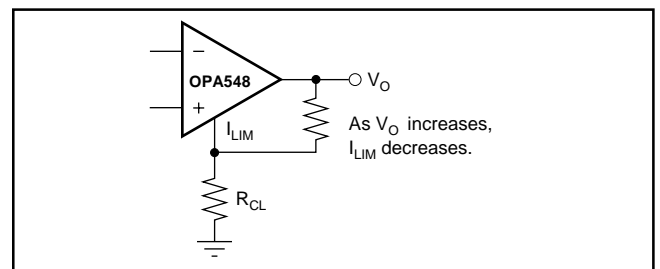
FIGURE 20. Single Quadrant V • I Limiting.

$$G = 1 + \frac{4k\Omega}{1k\Omega} = 5^{(1)}$$
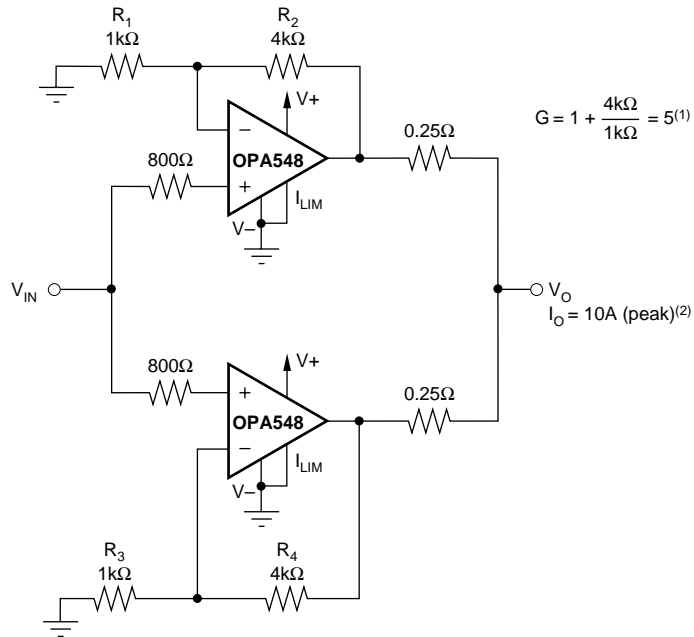
NOTES: (1) Works well for G < 10. Input offset causes output current to flow between amplifiers with G > 10. Gains (resistor ratios) of the two amplifiers should be carefully matched to ensure equal current sharing. (2) As configured (I_{LIM} connected to V–) output current limit is set to 10A (peak). Each amplifier is limited to 5A (peak). Other current limit values may be obtained, see Figure 3, "Adjustable Current Limit".

FIGURE 21. Parallel Output for Increased Output Current.

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ORDERABLE DEVICE	STATUS(1)	PACKAGE TYPE	PACKAGE DRAWING	PINS	PACKAGE QTY
OPA548F	OBSOLETE	PFM	KTW	7	
OPA548F/500	ACTIVE	PFM	KTW	7	500
OPA548FKTWT	ACTIVE	PFM	KTW	7	50
OPA548T	ACTIVE	PFM	KV	7	49
OPA548T-1	ACTIVE	TO/SOT	KC	7	49

(1) The marketing status values are defined as follows:
ACTIVE: Product device recommended for new designs.
LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.
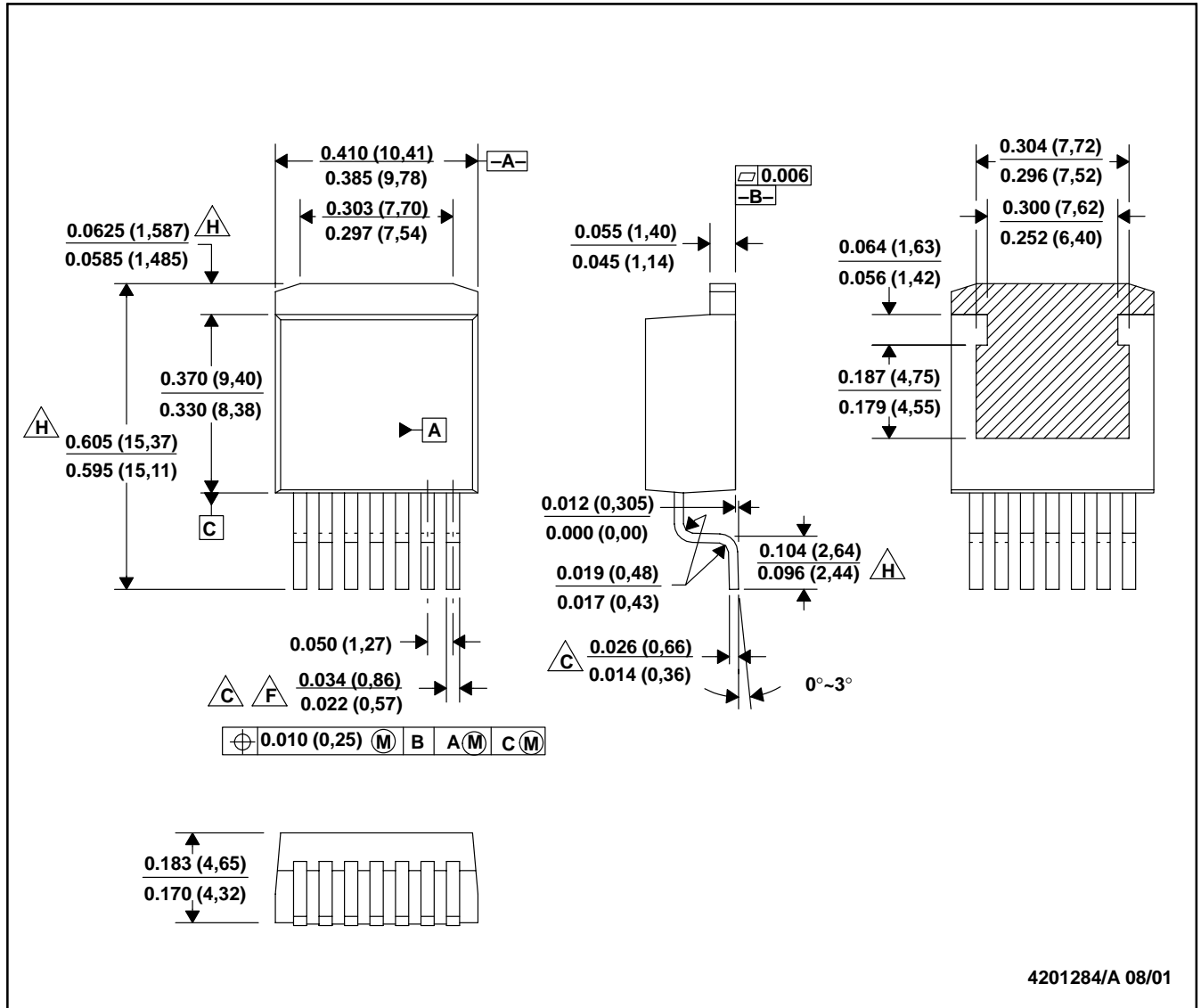**NRND:** Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.
PREVIEW: Device has been announced but is not in production. Samples may or may not be available.
OBSOLETE: TI has discontinued the production of the device.

KTW (R-PSFM-G7)   **PLASTIC FLANGE-MOUNT**

4201284/A 08/01

NOTES: A. All linear dimensions are in inches (millimeters).
  B. This drawing is subject to change without notice.
  C. Lead width and height dimensions apply to the plated lead.
  D. Leads are not allowed above the Datum B.
  E. Stand–off height is measured from lead tip with reference to Datum B.
  F. Lead width dimension does not include dambar protrusion. Allowable dambar protrusion shall not cause the lead width to exceed the maximum dimension by more than 0.003".
  G. Cross–hatch indicates exposed metal surface.
  H. Falls within JEDEC MO–169 with the exception of the dimensions indicated.

KC (R-PSFM-T7)   **PLASTIC FLANGE-MOUNT PACKAGE**

0.420 (10,67) / 0.380 (9,65)

0.156 (3,96) / 0.146 (3,71) **DIA**

0.113 (2,87) / 0.103 (2,62)

0.147 (3,73) / 0.137 (3,48)

1

7

0.125 (3,18)
(see Note C)

0.030 (0,76) / 0.026 (0,66)

0.050 (1,27)

⊕ 0.010 (0,25) Ⓜ

0.300 (7,62)

0.185 (4,70) / 0.175 (4,46)

0.055 (1,40) / 0.045 (1,14)

0.335 (8,51) / 0.325 (8,25)

1.020 (25,91) / 1.000 (25,40)

0.122 (3,10) / 0.102 (2,59)

0.025 (0,64) / 0.012 (0,30)

4040251 / B 01/95
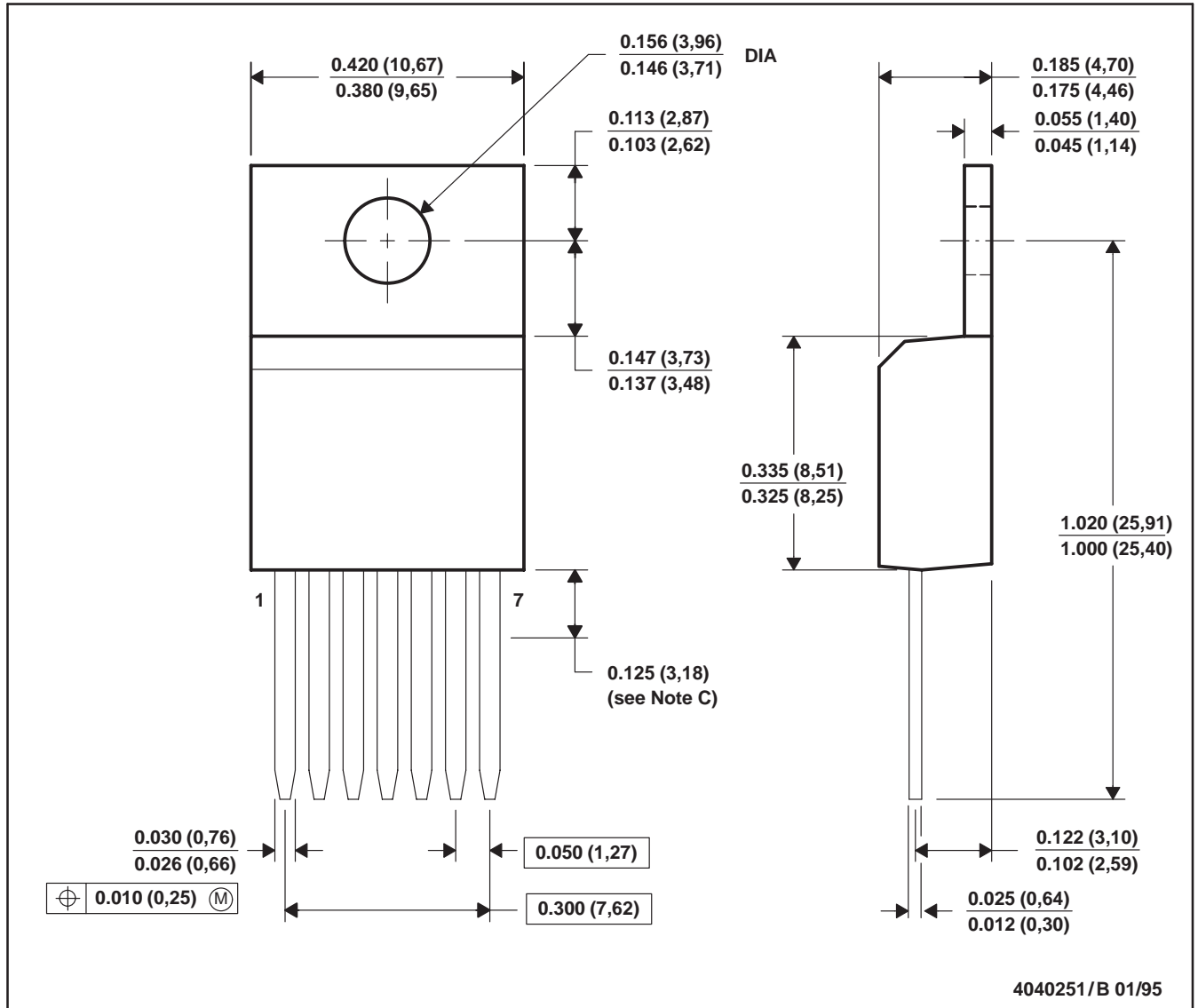
NOTES: A. All linear dimensions are in inches (millimeters).
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   C. Lead dimensions are not controlled within this area.
   D. All lead dimensions apply before solder dip.
   E. The center lead is in electrical contact with the mounting tab.

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1

0.420 (10,67)
0.380 (9,65)

0.156 (3,96)
0.146 (3,71)   DIA

0.113 (2,87)
0.103 (2,62)

0.147 (3,73)
0.137 (3,48)

0.335 (8,51)
0.325 (8,25)

0.120 (3,05)
0.110 (2,79)
(See Note C)

1   7

0.030 (0,76)
0.026 (0,66)

⊕ 0.010 (0,25) Ⓜ

0.050 (1,27)

0.300 (7,62)

0.185 (4,70)
0.175 (4,46)

0.055 (1,40)
0.045 (1,14)

0.692 (17,58)
0.682 (17,32)

0.822 (20,88)
0.812 (20,62)

0.122 (3,10)
0.102 (2,59)

0.025 (0,64)
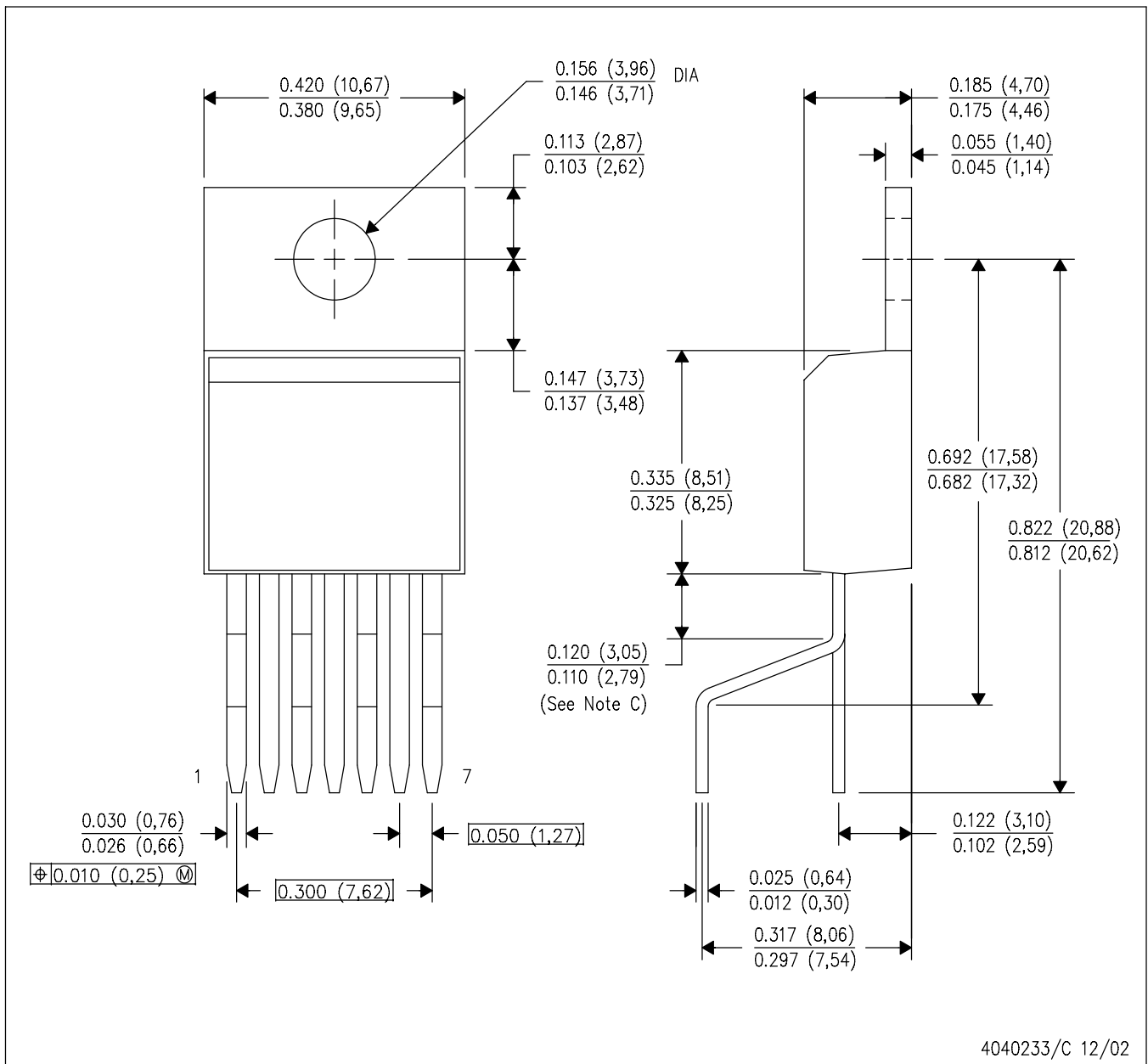0.012 (0,30)

0.317 (8,06)
0.297 (7,54)

4040233/C 12/02

NOTES: A. All linear dimensions are in inches (millimeters).
          B. This drawing is subject to change without notice.
          C. Lead dimensions are not controlled within this area.
          D. All dimensions apply before solder dip.
          E. The center lead is in electrical contact with the mounting tab.

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