

### LM4562

# Dual High Performance, High Fidelity Audio Operational Amplifier

## **General Description**

The LM4562 is part of the ultra-low distortion, low noise, high slew rate operational amplifier series optimized and fully specified for high performance, high fidelity applications. Combining advanced leading-edge process technology with state-of-the-art circuit design, the LM4562 audio operational amplifiers deliver superior audio signal amplification for outstanding audio performance. The LM4562 combines extremely low voltage noise density (2.7nV/VHz) with vanishingly low THD+N (0.00003%) to easily satisfy the most demanding audio applications. To ensure that the most challenging loads are driven without compromise, the LM4562 has a high slew rate of ±20V/µs and an output current capability of ±26mA. Further, dynamic range is maximized by an output stage that drives  $2k\Omega$  loads to within 1V of either power supply voltage and to within 1.4V when driving 600Q loads.

The LM4562's outstanding CMRR (120dB), PSRR (120dB), and  $\rm V_{OS}$  (0.1mV) give the amplifier excellent operational amplifier DC performance.

The LM4562 has a wide supply range of ±2.5V to ±17V. Over this supply range the LM4562's input circuitry maintains excellent common-mode and power supply rejection, as well as maintaining its low input bias current. The LM4562 is unity gain stable. This Audio Operational Amplifier achieves outstanding AC performance while driving complex loads with values as high as 100pF.

The LM4562 is available in 8-lead narrow body SOIC, 8-lead Plastic DIP and 8-lead Metal Can TO-99. Demonstration boards are available for each package.

# **Key Specifications**

■ Power Supply Voltage Range ±2.5V to ±17V

$R_L = 2k\Omega$	0.00003% (typ)
$R_L = 600\Omega$	0.00003% (typ)
■ Input Noise Density	2.7nV/√Hz (typ)
■ Slew Rate	±20V/μs (typ)
■ Gain Bandwidth Product	55MHz (typ)

■ THD+N ( $A_V = 1$ ,  $V_{OUT} = 3V_{BMS}$ ,  $f_{IN} = 1$ kHz)

■ Open Loop Gain (R<sub>L</sub> = 600Ω)
 Input Bias Current
 Input Offset Voltage
 140dB (typ)
 10nA (typ)
 0.1mV (typ)

■ DC Gain Linearity Error 0.000009%

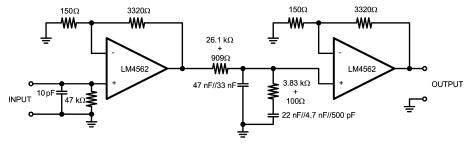
### **Features**

- Easily drives 600Ω loads
- Optimized for superior audio signal fidelity
- Output short circuit protection
- PSRR and CMRR exceed 120dB (typ)
- SOIC, DIP, TO-99 metal can packages

### **Applications**

- Ultra high quality audio amplification
- High fidelity preamplifiers
- High fidelity multimedia
- State of the art phono pre amps
- High performance professional audio
- High fidelity equalization and crossover networks
- High performance line drivers
- High performance line receivers
- High fidelity active filters

# **Typical Application**



Note: 1% metal film resistors, 5% polypropylene capacitors

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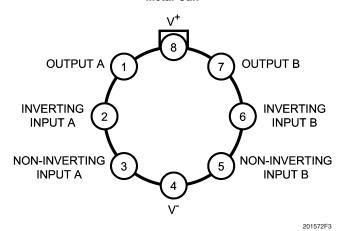
Passively Equalized RIAA Phono Preamplifier

# **Connection Diagrams**

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Order Number LM4562MA
See NS Package Number — M08A
Order Number LM4562NA
See NS Package Number — N08E

#### **Metal Can**



Order Number LM4562HA See NS Package Number — H08C

<b>Absolute Maximum Ratings</b> (Notes 1,	. 2	(Notes 1.	Ratings	Maximum	Absolute
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If Military/Aerospace specified devices are required, please contact the National Semiconductor Sales Office/ Distributors for availability and specifications.

Power Supply Voltage	
$(V_S = V^+ - V^-)$	36V
Storage Temperature	-65°C to 150°C
Input Voltage	(V-) - 0.7V  to  (V+) + 0.7V
Output Short Circuit (Note 3)	Continuous
Power Dissipation	Internally I imited

ESD Susceptibility (Note 4)	2000V
ESD Susceptibility (Note 5)	
Pins 1, 4, 7 and 8	200V
Pins 2, 3, 5 and 6	100V
Junction Temperature	150°C
Thermal Resistance	
$\theta_{JA}$ (SO)	145°C/W
$\theta_{JA}$ (NA)	102°C/W
$\theta_{JA}$ (HA)	150°C/W
$\theta_{JC}$ (HA)	35°C/W
Temperature Range	

 $T_{MIN} \le T_A \le T_{MAX}$   $-40^{\circ}C \le T_A \le 85^{\circ}C$ Supply Voltage Range  $\pm 2.5V \le V_S \le \pm 17V$ 

### **Electrical Characteristics for the LM4562** (Note 1)

The following specifications apply for the circuit shown in Figure X.  $V_S = \pm 15 V$ ,  $R_L = 2 k \Omega$ ,  $R_{SOURCE} = 10 \Omega$ ,  $f_{IN} = 1 k Hz$ , and  $T_A = 25 ^{\circ} C$ , unless otherwise specified.

			LM4562		Linita
Symbol	Parameter	Conditions	Typical	Limit	Units (Limits)
			(Note 6)	(Note 7)	(Lillins)
THD+N	Total Harmonic Distortion + Noise	$A_{V} = 1, V_{OUT} = 3V_{rms}$ $R_{L} = 2k\Omega$ $R_{L} = 600\Omega$	0.00003 0.00003	0.00009	% (max)
IMD	Intermodulation Distortion	$A_V = 1$ , $V_{OUT} = 3V_{RMS}$ Two-tone, 60kHz & 7kHz 4:1	0.00005		dB
GBWP	Gain Bandwidth Product		55	45	MHz (min)
SR	Slew Rate		±20	±15	V/μs (min)
FPBW	Full Power Bandwidth	V <sub>OUT</sub> = 1V <sub>P-P</sub> , -3dB referenced to output magnitude at f = 1kHz	10		MHz
t <sub>s</sub>	Settling time	$A_V = -1$ , 10V step, $C_L = 100$ pF 0.1% error range	1.2		μs
	Equivalent Input Noise Voltage	f <sub>BW</sub> = 20Hz to 20kHz	0.34	0.65	μV <sub>RMS</sub> (max)
e <sub>n</sub>	Equivalent Input Noise Density	f = 1kHz f = 10Hz	2.7 6.4	4.7	nV/√Hz (max)
i <sub>n</sub>	Current Noise Density	f = 1kHz f = 10Hz	1.6 3.1		p <b>A/</b> √Hz
Vos	Offset Voltage		±0.1	±0.7	mV (max)
$\Delta V_{OS}/\Delta Temp$	Average Input Offset Voltage Drift vs Temperature	$-40^{\circ}\text{C} \le \text{T}_{\text{A}} \le 85^{\circ}\text{C}$	0.2		μV/°C
PSRR	Average Input Offset Voltage Shift vs Power Supply Voltage	ΔV <sub>S</sub> = 20V (Note 8)	120	110	dB (min)
ISO <sub>CH-CH</sub>	Channel-to-Channel Isolation	$f_{IN} = 1kHz$ $f_{IN} = 20kHz$	118 112		dB
I <sub>B</sub>	Input Bias Current	V <sub>CM</sub> = 0V	10	72	nA (max)
$\Delta I_{OS}/\Delta Temp$	Input Bias Current Drift vs Temperature	$-40^{\circ}\text{C} \le \text{T}_{\text{A}} \le 85^{\circ}\text{C}$	0.1		nA/°C
I <sub>os</sub>	Input Offset Current	$V_{CM} = 0V$	11	65	nA (max)
V <sub>IN-CM</sub>	Common-Mode Input Voltage Range		+14.1 -13.9	(V+) - 2.0 (V-) + 2.0	V (min)
CMRR	Common-Mode Rejection	-10V <vcm<10v< td=""><td>120</td><td>110</td><td>dB (min)</td></vcm<10v<>	120	110	dB (min)

### **Electrical Characteristics for the LM4562** (Note 1)

The following specifications apply for the circuit shown in Figure X.  $V_S = \pm 15V$ ,  $R_L = 2k\Omega$ ,  $R_{SOURCE} = 10\Omega$ ,  $f_{IN} = 1kHz$ , and  $T_A = 25^{\circ}C$ , unless otherwise specified. (Continued)

			LM4562		11.21.
Symbol	Parameter	Conditions	Typical	Limit	Units (Limits)
			(Note 6)	(Note 7)	(Limits)
7	Differential Input Impedance		30		kΩ
$Z_{IN}$	Common Mode Input Impedance	-10V <vcm<10v< td=""><td>1000</td><td></td><td>MΩ</td></vcm<10v<>	1000		MΩ
		$-10V$ <vout<10v, r<sub="">L = <math>600\Omega</math></vout<10v,>	140	125	
$A_{VOL}$	Open Loop Voltage Gain	$-10V < Vout < 10V, R_L = 2k\Omega$	140		dB (min)
		$-10V < Vout < 10V, R_L = 10k\Omega$	140		1
		$R_L = 600\Omega$	±13.6	±12.5	
$V_{OUTMAX}$	Maximum Output Voltage Swing	$R_L = 2k\Omega$	±14.0		V (min)
		$R_L = 10k\Omega$	±14.1		1
I <sub>OUT</sub>	Output Current	$R_L = 600\Omega, V_S = \pm 17V$	±26	±23	mA (min)
	Instantaneous Short Circuit Current		+53		m Λ
I <sub>OUT-CC</sub>	Instantaneous Short Circuit Current		-42		mA
		$f_{IN} = 10kHz$			
R <sub>OUT</sub>	Output Impedance	Closed-Loop	0.01		Ω
		Open-Loop	13		
$C_{LOAD}$	Capacitive Load Drive Overshoot	100pF	16		%
I <sub>S</sub>	Total Quiescent Current	I <sub>OUT</sub> = 0mA	10	12	mA (max)

Note 1: Absolute Maximum Ratings indicate limits beyond which damage to the device may occur.

**Note 2:** Operating Ratings indicate conditions for which the device is functional, but do not guarantee specific performance limits. For guaranteed specifications and test conditions, see the Electrical Characteristics. The guaranteed specifications apply only for the test conditions listed. Some performance characteristics may degrade when the device is not operated under the listed test conditions.

Note 3: Amplifier output connected to GND, any number of amplifiers within a package.

Note 4: Human body model, 100pF discharged through a  $1.5k\Omega$  resistor.

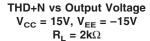
**Note 5:** Machine Model ESD test is covered by specification EIAJ IC-121-1981. A 200pF cap is charged to the specified voltage and then discharged directly into the IC with no external series resistor (resistance of discharge path must be under  $50\Omega$ ).

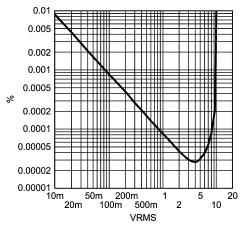
Note 6: Typical specifications are specified at +25°C and represent the most likely parametric norm.

Note 7: Tested limits are guaranteed to National's AOQL (Average Outgoing Quality Level).

Note 8: PSRR is measured as follows:  $V_{OS}$  is measured at two supply voltages,  $\pm 5V$  and  $\pm 15V$ . PSRR =  $|20log(\Delta V_{OS}/\Delta V_S)|$ .

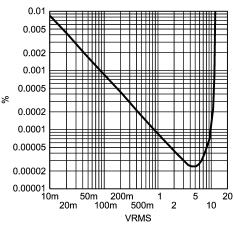
## **Typical Performance Characteristics**





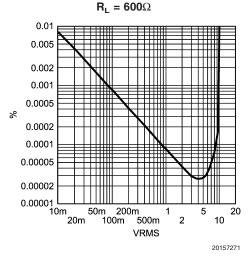
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THD+N vs Output Voltage  $V_{CC}$  = 17V,  $V_{EE}$  = -17V  $R_L$  = 2k $\Omega$ 

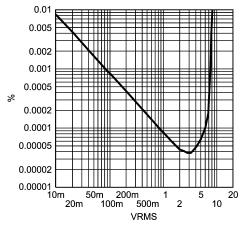


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THD+N vs Output Voltage V<sub>CC</sub> = 15V, V<sub>EE</sub> = -15V

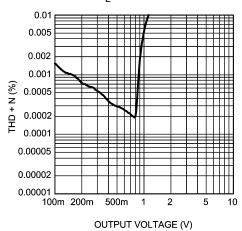


THD+N vs Output Voltage  $V_{CC}$  = 12V,  $V_{EE}$  = -12V  $R_L$  = 2k $\Omega$ 



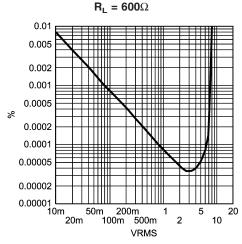
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THD+N vs Output Voltage  $V_{CC}$  = 2.5V,  $V_{EE}$  = -2.5V  $R_L$  =  $2k\Omega$ 



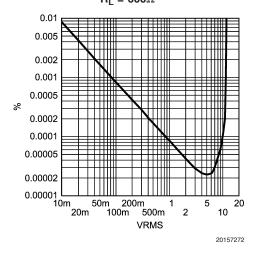
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THD+N vs Output Voltage  $V_{CC} = 12V$ ,  $V_{EE} = -12V$ 

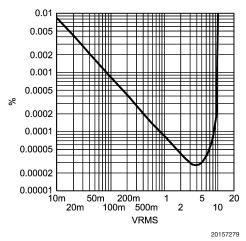


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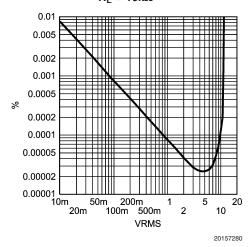
THD+N vs Output Voltage  $\begin{aligned} \text{V}_{\text{CC}} &= 17\text{V}, \ \text{V}_{\text{EE}} = -17\text{V} \\ \text{R}_{\text{L}} &= 600\Omega \end{aligned}$ 



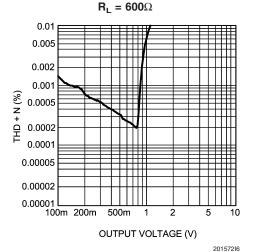
THD+N vs Output Voltage  $V_{CC}$  = 15V,  $V_{EE}$  = -15V  $R_L$  = 10k $\Omega$ 



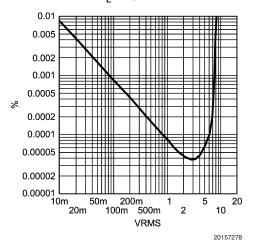
THD+N vs Output Voltage  $V_{CC}$  = 17V,  $V_{EE}$  = -17V  $R_L$  = 10k $\Omega$ 



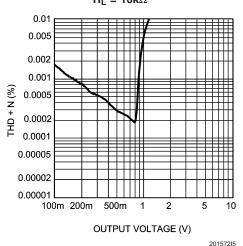
THD+N vs Output Voltage  $V_{CC} = 2.5V$ ,  $V_{EE} = -2.5V$ 



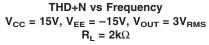
THD+N vs Output Voltage  $V_{CC}$  = 12V,  $V_{EE}$  = -12V  $R_L$  = 10k $\Omega$ 

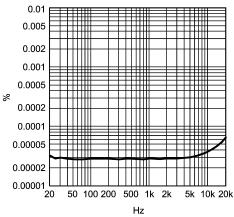


THD+N vs Output Voltage  $\label{eq:VCC} \begin{aligned} \text{V}_{\text{CC}} &= 2.5\text{V}, \ \text{V}_{\text{EE}} = -2.5\text{V} \\ \text{R}_{\text{L}} &= 10\text{k}\Omega \end{aligned}$ 



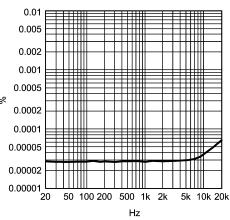
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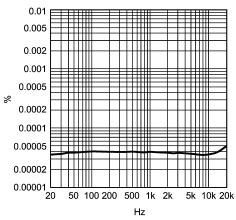
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# THD+N vs Frequency $V_{CC}$ = 17V, $V_{EE}$ = -17V, $V_{OUT}$ = $3V_{RMS}$ $R_L$ = $2k\Omega$



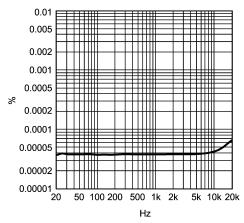
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THD+N vs Frequency  $\begin{aligned} \text{V}_{\text{CC}} &= \text{12V}, \, \text{V}_{\text{EE}} = -\text{12V}, \, \text{V}_{\text{OUT}} = \text{3V}_{\text{RMS}} \\ \text{R}_{\text{L}} &= 600\Omega \end{aligned}$ 



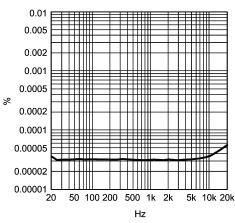
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THD+N vs Frequency  $V_{CC} = 12V$ ,  $V_{EE} = -12V$ ,  $V_{OUT} = 3V_{RMS}$   $R_{c} = 2kO$ 



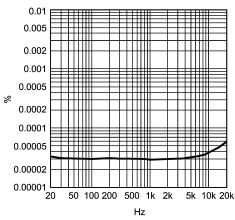
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THD+N vs Frequency  $\begin{aligned} \text{V}_{\text{CC}} &= \text{15V}, \ \text{V}_{\text{EE}} = -\text{15V}, \ \text{V}_{\text{OUT}} = \text{3V}_{\text{RMS}} \\ \text{R}_{\text{L}} &= 600\Omega \end{aligned}$ 

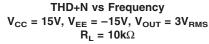


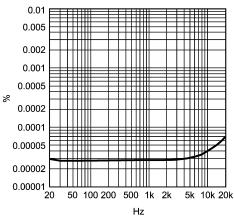
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THD+N vs Frequency  $\begin{aligned} \text{V}_{\text{CC}} &= \text{17V}, \, \text{V}_{\text{EE}} = -\text{17V}, \, \text{V}_{\text{OUT}} = \text{3V}_{\text{RMS}} \\ \text{R}_{\text{L}} &= 600\Omega \end{aligned}$ 



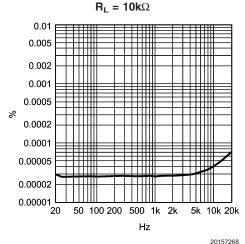
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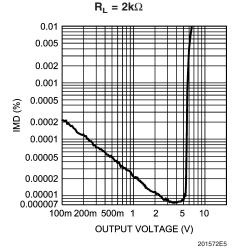


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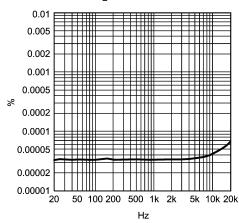
THD+N vs Frequency  $V_{CC} = 17V$ ,  $V_{EE} = -17V$ ,  $V_{OUT} = 3V_{RMS}$ 



IMD vs Output Voltage  $V_{CC} = 12V$ ,  $V_{EE} = -12V$ 

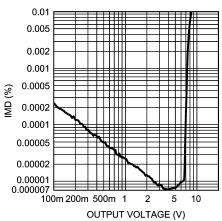


THD+N vs Frequency  $\begin{aligned} \text{V}_{\text{CC}} &= \text{12V}, \, \text{V}_{\text{EE}} = -\text{12V}, \, \text{V}_{\text{OUT}} = \text{3V}_{\text{RMS}} \\ \text{R}_{\text{L}} &= \text{10k}\Omega \end{aligned}$ 



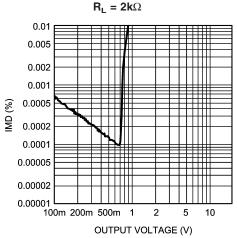
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 $\begin{aligned} & \text{IMD vs Output Voltage} \\ & \text{V}_{\text{CC}} = \text{15V}, \, \text{V}_{\text{EE}} = -\text{15V} \\ & \text{R}_{\text{L}} = \text{2k}\Omega \end{aligned}$ 

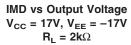


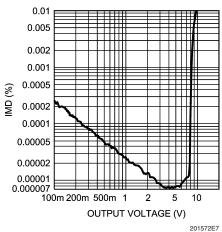
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IMD vs Output Voltage  $V_{CC} = 2.5V$ ,  $V_{EE} = -2.5V$ 

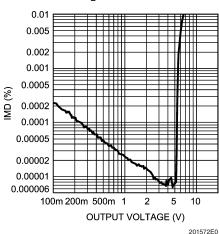


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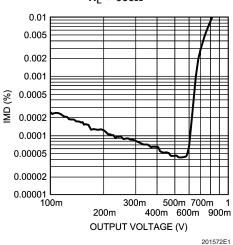




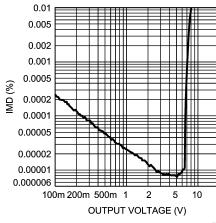
IMD vs Output Voltage  $V_{CC}$  = 12V,  $V_{EE}$  = -12V  $R_L$  = 600 $\Omega$ 



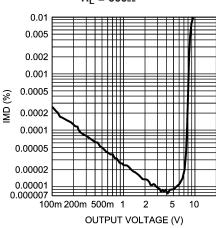
IMD vs Output Voltage  $V_{CC}$  = 2.5V,  $V_{EE}$  = -2.5V  $R_L$  = 600 $\Omega$ 



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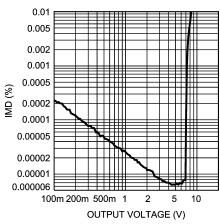


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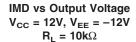


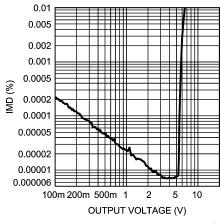
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IMD vs Output Voltage  $V_{CC}$  = 15V,  $V_{EE}$  = -15V  $R_L$  = 10k $\Omega$ 



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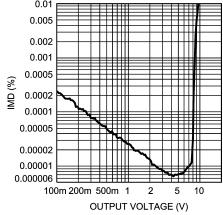




 $R_L = 10k\Omega$ 0.01

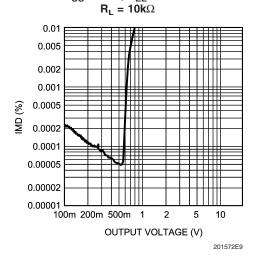
**IMD** vs Output Voltage

 $V_{CC} = 17V$ ,  $V_{EE} = -17V$ 

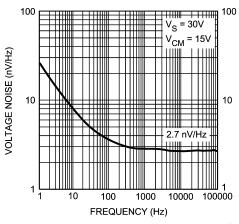


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**IMD** vs Output Voltage  $V_{CC}$  = 2.5V,  $V_{EE}$  = -2.5V

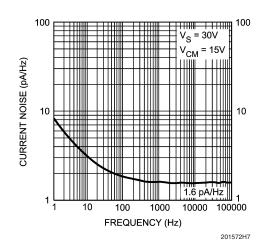


Voltage Noise Density vs Frequency

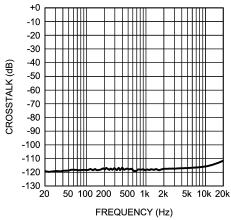


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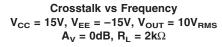
#### **Current Noise Density vs Frequency**

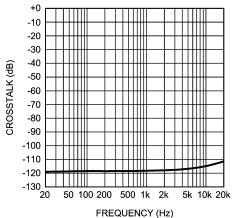


Crosstalk vs Frequency  $V_{CC}$  = 15V,  $V_{EE}$  = -15V,  $V_{OUT}$  =  $3V_{RMS}$   $A_V$  = 0dB,  $R_L$  =  $2k\Omega$ 



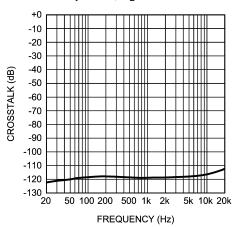
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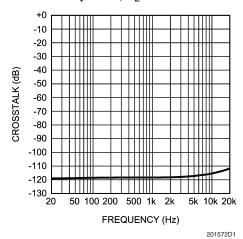
201572C9

#### Crosstalk vs Frequency $V_{CC} = 12V, V_{EE} = -12V, V_{OUT} = 10V_{RMS}$ $A_V = 0$ dB, $R_L = 2$ k $\Omega$

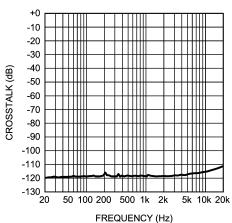


201572C7

### Crosstalk vs Frequency $V_{CC} = 17V, V_{EE} = -17V, V_{OUT} = 10V_{RMS}$ $A_V = 0$ dB, $R_L = 2$ k $\Omega$

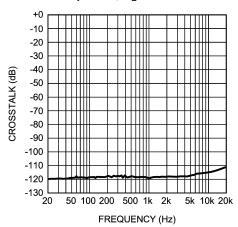


Crosstalk vs Frequency  $V_{CC}$  = 12V,  $V_{EE}$  = -12V,  $V_{OUT}$  =  $3V_{RMS}$  $A_V = 0$ dB,  $R_I = 2$ k $\Omega$ 



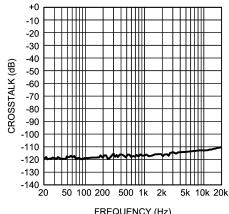
201572C6

Crosstalk vs Frequency  $V_{CC} = 17V$ ,  $V_{EE} = -17V$ ,  $V_{OUT} = 3V_{RMS}$  $A_V = 0$ dB,  $R_L = 2$ k $\Omega$ 



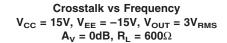
201572D0

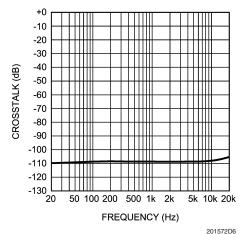
Crosstalk vs Frequency  $V_{CC}$  = 2.5V,  $V_{EE}$  = -2.5V,  $V_{OUT}$  = 1 $V_{RMS}$  $A_V = 0$ dB,  $R_L = 2k\Omega$ 



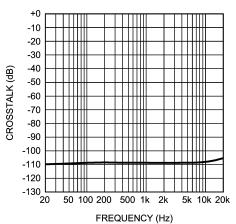
FREQUENCY (Hz)

201572C4



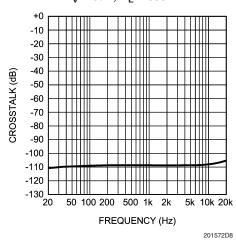


$$\begin{aligned} & \text{Crosstalk vs Frequency} \\ \text{V}_{\text{CC}} &= \text{12V}, \, \text{V}_{\text{EE}} = -\text{12V}, \, \text{V}_{\text{OUT}} = \text{3V}_{\text{RMS}} \\ & \text{A}_{\text{V}} = \text{0dB}, \, \text{R}_{\text{L}} = 600\Omega \end{aligned}$$

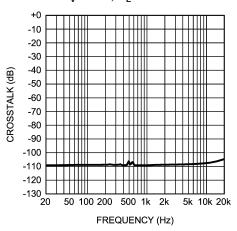


201572D4

Crosstalk vs Frequency  $V_{CC} = 17V$ ,  $V_{EE} = -17V$ ,  $V_{OUT} = 3V_{RMS}$  $A_V = 0$ dB,  $R_L = 600$  $\Omega$ 

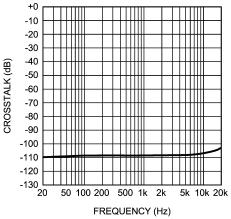


Crosstalk vs Frequency  $V_{CC} = 15V, V_{EE} = -15V, V_{OUT} = 10V_{RMS}$  $A_V = 0 dB$ ,  $R_I = 600 \Omega$ 



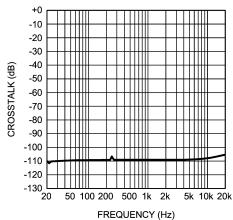
201572D7

Crosstalk vs Frequency  $V_{CC} = 12V, V_{EE} = -12V, V_{OUT} = 10V_{RMS}$  $A_V = 0$ dB,  $R_L = 600\Omega$ 

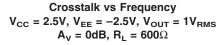


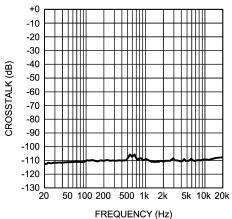
201572D5

Crosstalk vs Frequency  $V_{CC} = 17V$ ,  $V_{EE} = -17V$ ,  $V_{OUT} = 10V_{RMS}$  $A_V = 0$ dB,  $R_L = 600$  $\Omega$ 



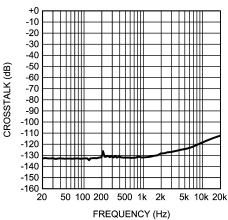
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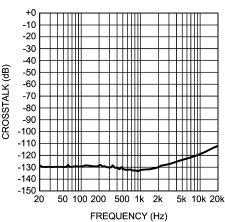
201572D2

Crosstalk vs Frequency  $\begin{aligned} &\textbf{V}_{\text{CC}} = \textbf{15V}, \, \textbf{V}_{\text{EE}} = -\textbf{15V}, \, \textbf{V}_{\text{OUT}} = \textbf{10V}_{\text{RMS}} \\ &\textbf{A}_{\text{V}} = \textbf{0dB}, \, \textbf{R}_{\text{L}} = \textbf{10k}\Omega \end{aligned}$ 



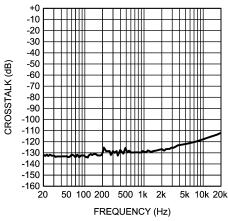
201572C1

Crosstalk vs Frequency  $\begin{aligned} &V_{\text{CC}} = 12\text{V, } V_{\text{EE}} = -12\text{V, } V_{\text{OUT}} = 10\text{V}_{\text{RMS}} \\ &A_{\text{V}} = 0\text{dB, } R_{\text{L}} = 10\text{k}\Omega \end{aligned}$ 



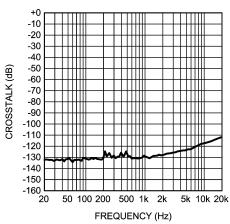
201572B9

Crosstalk vs Frequency  $\begin{aligned} \textbf{V}_{\text{CC}} &= \textbf{15V}, \, \textbf{V}_{\text{EE}} = -\textbf{15V}, \, \textbf{V}_{\text{OUT}} = \textbf{3V}_{\text{RMS}} \\ \textbf{A}_{\text{V}} &= \textbf{0dB}, \, \textbf{R}_{\text{I}} = \textbf{10k}\Omega \end{aligned}$ 



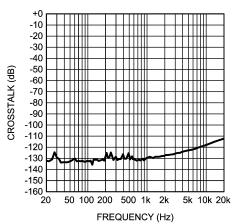
201572C0

 $\begin{aligned} & \text{Crosstalk vs Frequency} \\ & \text{V}_{\text{CC}} = \text{12V}, \, \text{V}_{\text{EE}} = -\text{12V}, \, \text{V}_{\text{OUT}} = \text{3V}_{\text{RMS}} \\ & \text{A}_{\text{V}} = \text{0dB}, \, \text{R}_{\text{L}} = \text{10k}\Omega \end{aligned}$ 

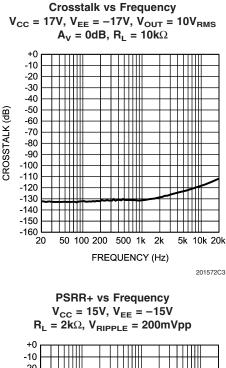


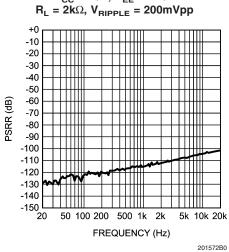
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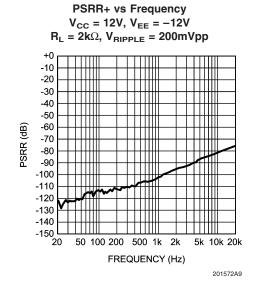
 $\begin{aligned} & \text{Crosstalk vs Frequency} \\ \text{V}_{\text{CC}} &= 17\text{V}, \, \text{V}_{\text{EE}} = -17\text{V}, \, \text{V}_{\text{OUT}} = 3\text{V}_{\text{RMS}} \\ & \text{A}_{\text{V}} = 0\text{dB}, \, \text{R}_{\text{L}} = 10\text{k}\Omega \end{aligned}$ 

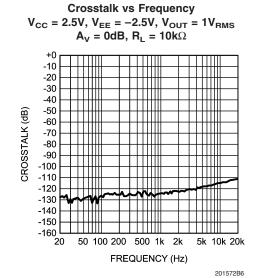


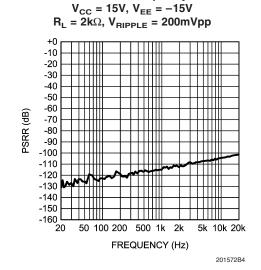
201572C2



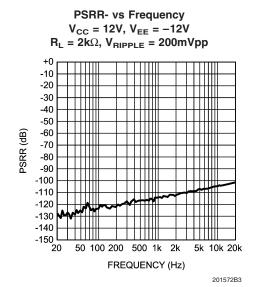


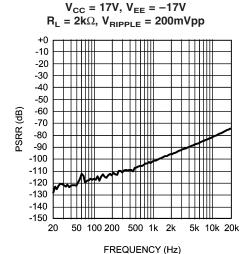






**PSRR- vs Frequency** 



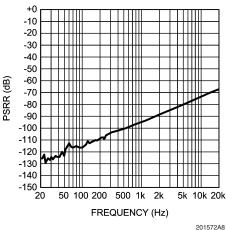


**PSRR+ vs Frequency** 

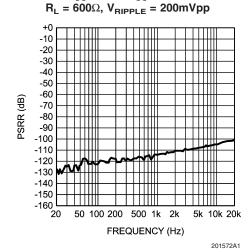
PSRR+ vs Frequency

201572J3



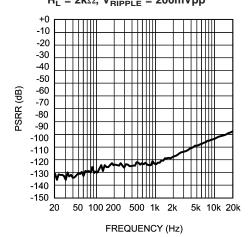


PSRR+ vs Frequency V<sub>CC</sub> = 15V, V<sub>CC</sub> = -15V



PSRR- vs Frequency

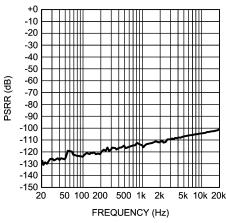




201572J2

PSRR- vs Frequency  $V_{CC} = 2.5V$ ,  $V_{EE} = -2.5V$ 

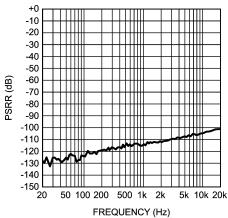




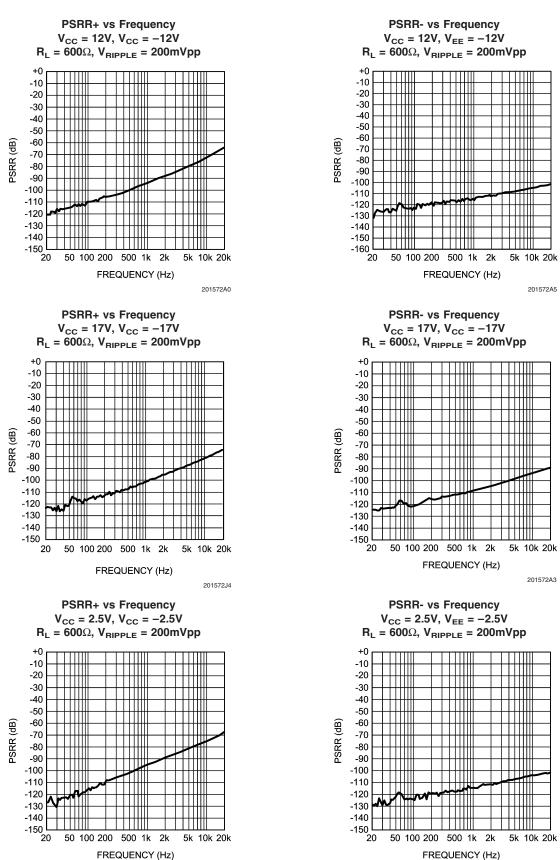
201572B2

### PSRR- vs Frequency

$$V_{CC}$$
 = 15V,  $V_{EE}$  = -15V   
R<sub>L</sub> = 600 $\Omega$ ,  $V_{RIPPLE}$  = 200mVpp

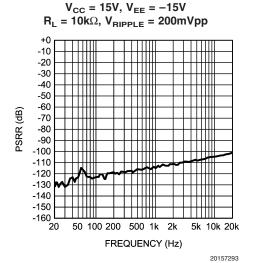


201572A6



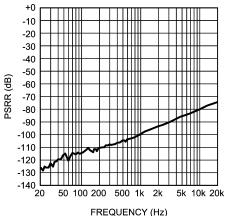
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201572A4



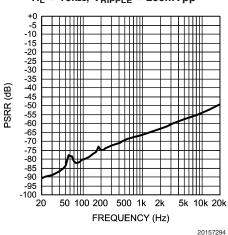
**PSRR+ vs Frequency** 



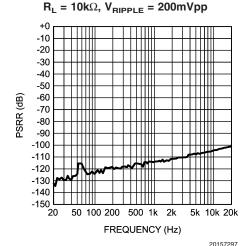


PSRR+ vs Frequency  $V_{CC}$  = 17V,  $V_{EE}$  = -17V  $R_L$  = 10k $\Omega$ ,  $V_{RIPPLE}$  = 200mVpp

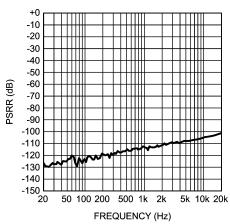
20157292



PSRR- vs Frequency V<sub>CC</sub> = 15V, V<sub>EE</sub> = -15V

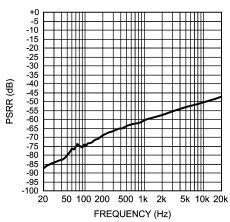




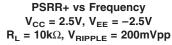


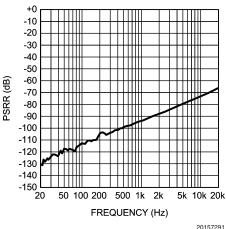
20157296

PSRR- vs Frequency  $V_{CC}$  = 17V,  $V_{EE}$  = -17V  $R_L$  = 10k $\Omega$ ,  $V_{RIPPLE}$  = 200mVpp

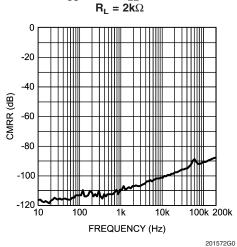


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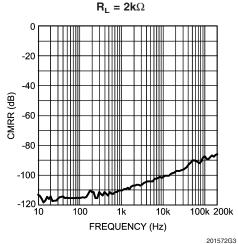




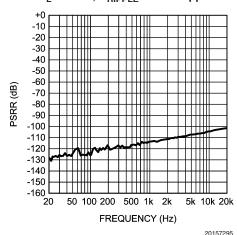
CMRR vs Frequency V<sub>CC</sub> = 15V, V<sub>EE</sub> = -15V



CMRR vs Frequency V<sub>CC</sub> = 17V, V<sub>EE</sub> = -17V

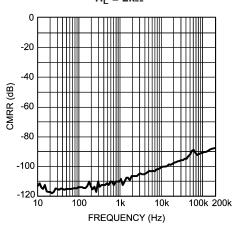


$$\begin{split} & \text{PSRR- vs Frequency} \\ & \text{V}_{\text{CC}} = 2.5\text{V}, \, \text{V}_{\text{EE}} = -2.5\text{V} \\ & \text{R}_{\text{L}} = 10\text{k}\Omega, \, \text{V}_{\text{RIPPLE}} = 200\text{mVpp} \end{split}$$



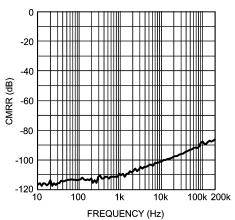
201572

CMRR vs Frequency  $V_{CC}$  = 12V,  $V_{EE}$  = -12V  $R_L$  = 2k $\Omega$ 



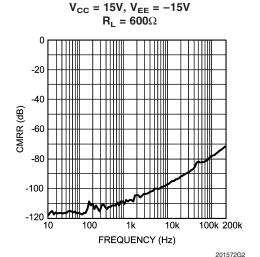
201572F7

CMRR vs Frequency  $V_{CC}$  = 2.5V,  $V_{EE}$  = -2.5V  $R_L$  = 2k $\Omega$ 

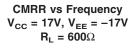


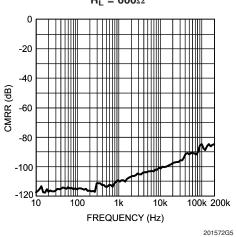
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201572F4

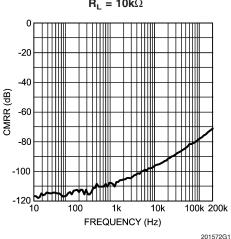


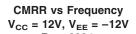
**CMRR** vs Frequency

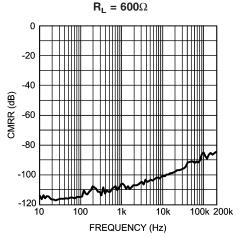




CMRR vs Frequency  $V_{CC}$  = 15V,  $V_{EE}$  = -15V  $R_L$  = 10k $\Omega$ 

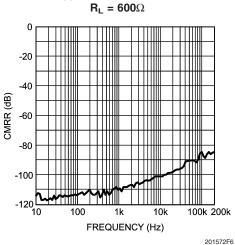




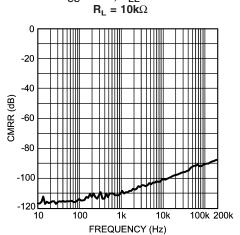


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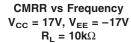
# CMRR vs Frequency $V_{CC} = 2.5V$ , $V_{EE} = -2.5V$

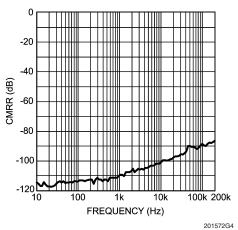


CMRR vs Frequency  $V_{CC} = 12V$ ,  $V_{EE} = -12V$ 

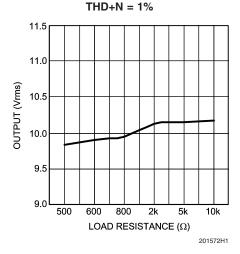


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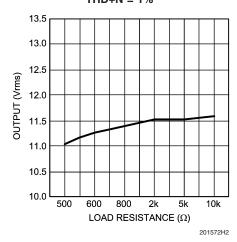




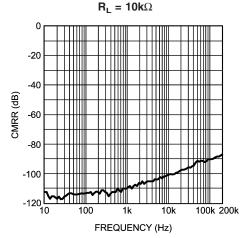
Output Voltage vs Load Resistance V<sub>DD</sub> = 15V, V<sub>EE</sub> = -15V



Output Voltage vs Load Resistance  $V_{DD} = 17V, V_{EE} = -17V$ THD+N = 1%

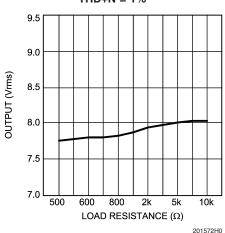


CMRR vs Frequency  $V_{CC} = 2.5V$ ,  $V_{EE} = -2.5V$ 

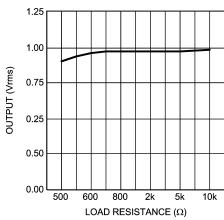


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# Output Voltage vs Load Resistance $V_{DD} = 12V, V_{EE} = -12V$ THD+N = 1%

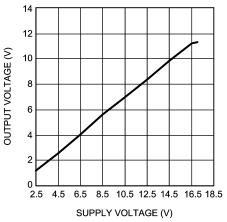


Output Voltage vs Load Resistance  $V_{DD}$  = 2.5V,  $V_{EE}$  = -2.5V THD+N = 1%



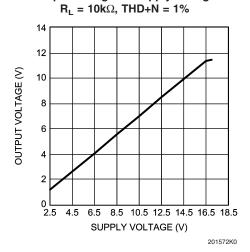
201572G9

# Output Voltage vs Supply Voltage $R_L = 2k\Omega$ , THD+N = 1%

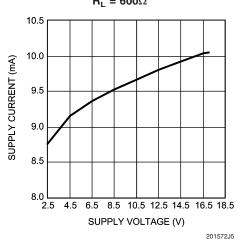


201572J9

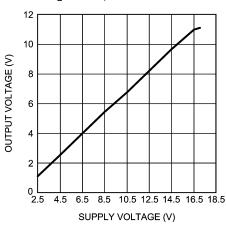
# Output Voltage vs Supply Voltage



# Supply Current vs Supply Voltage $R_{L} = 600 \Omega \label{eq:RL}$

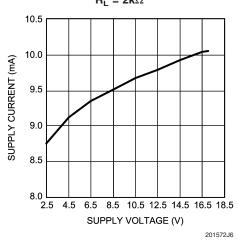


# Output Voltage vs Supply Voltage $R_L = 600\Omega$ , THD+N = 1%

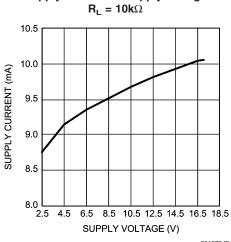


201572J8

# Supply Current vs Supply Voltage $\mathbf{R_L} = \mathbf{2} \mathbf{k} \boldsymbol{\Omega}$

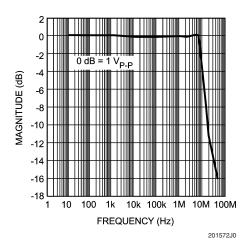


Supply Current vs Supply Voltage

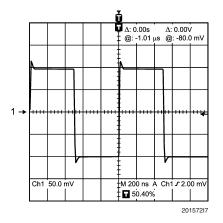


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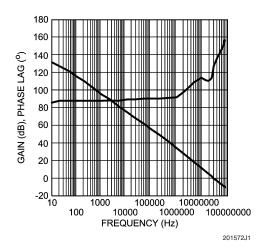
#### Full Power Bandwidth vs Frequency



Small-Signal Transient Response  $A_V = 1$ , CL = 10pF

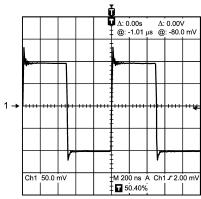


#### Gain Phase vs Frequency



Small-Signal Transient Response

$$A_V = 1$$
,  $CL = 100pF$ 



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### **Application Information**

#### **DISTORTION MEASUREMENTS**

The vanishingly low residual distortion produced by LM4562 is below the capabilities of all commercially available equipment. This makes distortion measurements just slightly more difficult than simply connecting a distortion meter to the amplifier's inputs and outputs. The solution, however, is quite simple: an additional resistor. Adding this resistor extends the resolution of the distortion measurement equipment.

The LM4562's low residual distortion is an input referred internal error. As shown in Figure 1, adding the  $10\Omega$  resistor connected between the amplifier's inverting and non-inverting inputs changes the amplifier's noise gain. The re-

sult is that the error signal (distortion) is amplified by a factor of 101. Although the amplifier's closed-loop gain is unaltered, the feedback available to correct distortion errors is reduced by 101, which means that measurement resolution increases by 101. To ensure minimum effects on distortion measurements, keep the value of R1 low as shown in Figure 1.

This technique is verified by duplicating the measurements with high closed loop gain and/or making the measurements at high frequencies. Doing so produces distortion components that are within the measurement equipment's capabilities. This datasheet's THD+N and IMD values were generated using the above described circuit connected to an Audio Precision System Two Cascade.

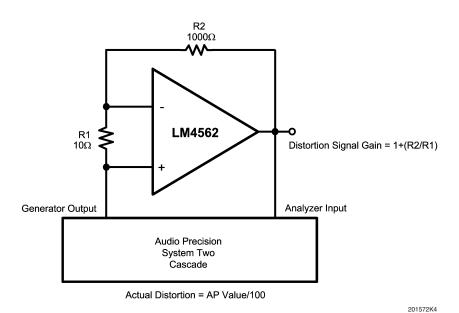
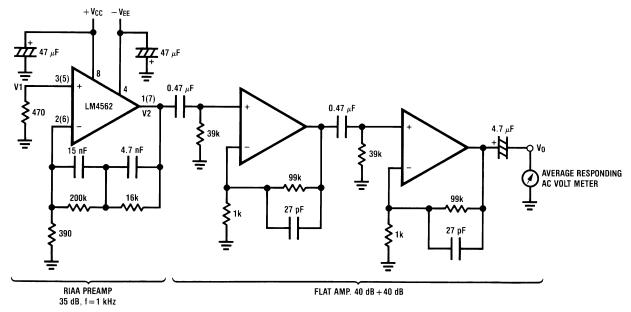


FIGURE 1. THD+N and IMD Distortion Test Circuit

#### NOISE MEASUREMENT CIRCUIT

The LM4562 is a high speed op amp with excellent phase margin and stability. Capacitive loads up to 100pF will cause little change in the phase characteristics of the amplifiers and are therefore allowable.

Capacitive loads greater than 100pF must be isolated from the output. The most straightforward way to do this is to put a resistor in series with the output. This resistor will also prevent excess power dissipation if the output is accidentally shorted.

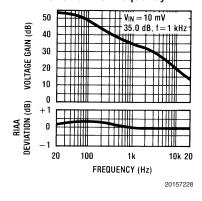


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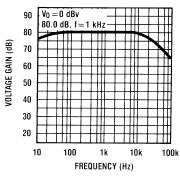
Complete shielding is required to prevent induced pick up from external sources. Always check with oscilloscope for power line noise.

Total Gain: 115 dB @f = 1 kHz Input Referred Noise Voltage: e<sub>n</sub> = V0/560,000 (V)

RIAA Preamp Voltage Gain, RIAA Deviation vs Frequency

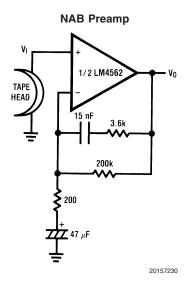


Flat Amp Voltage Gain vs Frequency

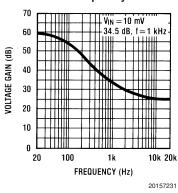


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#### **TYPICAL APPLICATIONS**

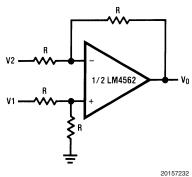


# NAB Preamp Voltage Gain vs Frequency

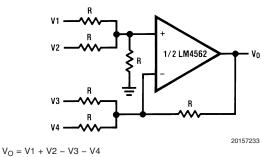


 $A_V = 34.5$  F = 1 kHz  $E_n = 0.38 \text{ }\mu\text{V}$  A Weighted

### **Balanced to Single Ended Converter**

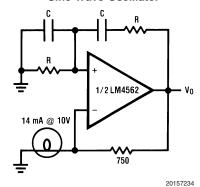


Adder/Subtracter



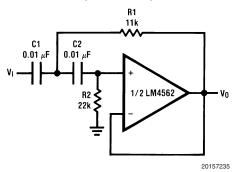
V<sub>O</sub> = V1-V2

#### Sine Wave Oscillator



 $f_0 = \frac{1}{0 - PC}$ 

# Second Order High Pass Filter (Butterworth)

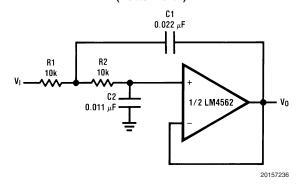


if 
$$C1 = C2 = C$$

$$R1 = \frac{\sqrt{2}}{2\omega_0 C}$$

Illustration is  $f_0 = 1 \text{ kHz}$ 

# Second Order Low Pass Filter (Butterworth)

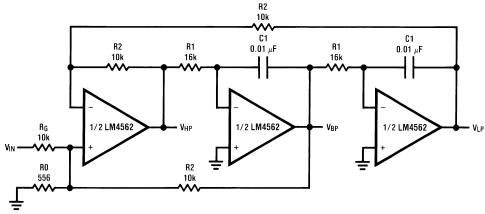


$$C1 = \frac{\sqrt{2}}{\omega_0 R}$$

$$C2 = \frac{C1}{2}$$

Illustration is  $f_0 = 1 \text{ kHz}$ 

#### State Variable Filter



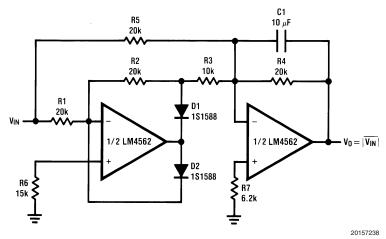
20157237

$$f_0 = \frac{1}{2\pi C1R1}, Q = \frac{1}{2} \left(1 + \frac{R2}{R0} + \frac{R2}{RG}\right), A_{BP} = QA_{LP} = QA_{LH} = \frac{R2}{RG}$$

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Illustration is  $f_0 = 1 \text{ kHz}$ , Q = 10,  $A_{BP} = 1$ 

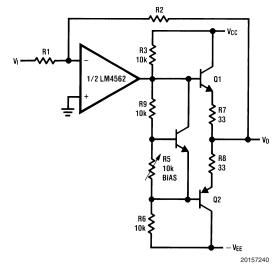
#### AC/DC Converter



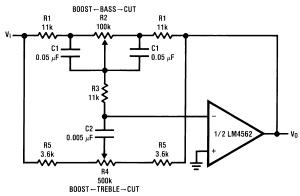
### 2 Channel Panning Circuit (Pan Pot)

# 3.41R1 51k R1 15k 15k 15k 172 LM4562 V<sub>02</sub> 1/2 LM4562 V<sub>02</sub> 3.41R1 51k 20157239

#### Line Driver



#### **Tone Control**

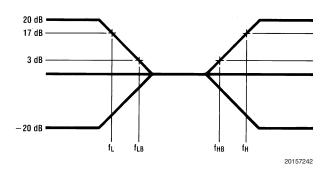


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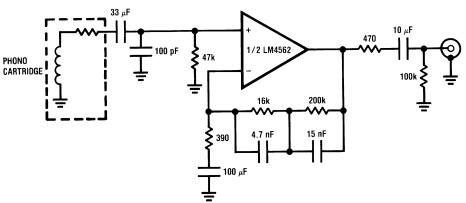
$$\begin{split} f_L &= \frac{1}{2\pi R2C1}, f_{LB} = \frac{1}{2\pi R1C1} \\ f_H &= \frac{1}{2\pi R5C2}, f_{HB} = \frac{1}{2\pi (R1 + R5 + 2R3)C2} \end{split}$$

Illustration is:

$$f_L = 32 \text{ Hz}, f_{LB} = 320 \text{ Hz}$$
  
 $f_H = 11 \text{ kHz}, f_{HB} = 1.1 \text{ kHz}$ 



### **RIAA Preamp**



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$$A_V = 35 \text{ dB}$$

$$E_n = 0.33 \ \mu V$$

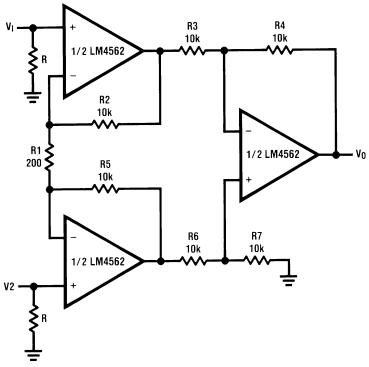
$$S/N = 90 dB$$

$$f = 1 \text{ kHz}$$

A Weighted, 
$$V_{IN} = 10 \text{ mV}$$

$$@f = 1 \text{ kHz}$$

### **Balanced Input Mic Amp**



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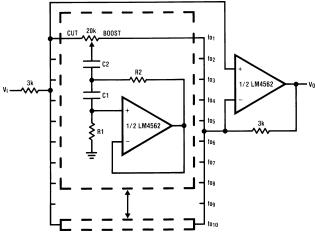
If R2 = R5, R3 = R6, R4 = R7  

$$V0 = \left(1 + \frac{2R2}{R1}\right) \frac{R4}{R3} (V2 - V1)$$

Illustration is:

V0 = 101(V2 - V1)

### 10 Band Graphic Equalizer



20157244

fo (Hz)	C <sub>1</sub>	C <sub>2</sub>	R <sub>1</sub>	R <sub>2</sub>
32	0.12µF	4.7µF	75kΩ	500Ω
64	0.056µF	3.3µF	68kΩ	510Ω
125	0.033µF	1.5µF	62kΩ	510Ω
250	0.015µF	0.82µF	68kΩ	470Ω
500	8200pF	0.39µF	62kΩ	470Ω
1k	3900pF	0.22µF	68kΩ	470Ω
2k	2000pF	0.1µF	68kΩ	470Ω
4k	1100pF	0.056µF	62kΩ	470Ω
8k	510pF	0.022µF	68kΩ	510Ω
16k	330pF	0.012µF	51kΩ	510Ω

Note 9: At volume of change =  $\pm 12 \text{ dB}$ 

Q = 1.

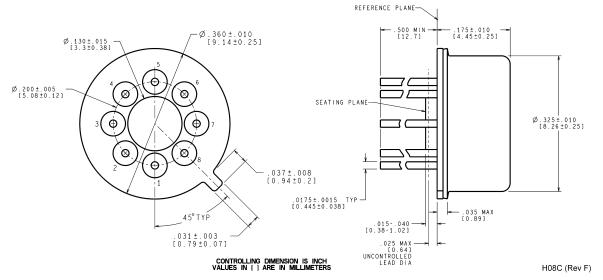
Reference: "AUDIO/RADIO HANDBOOK", National Semiconductor, 1980, Page 2-61

# **Revision History**

Rev	Date	Description	
0.05	5/24/05	Added edits and changes per TW	
		Chan's and M Koterasawa-san's	
		inputs and conference call	
		(5/20/05).	
		Changed part number to LM4562.	
0.10	5/25/05	Updates based on inputs from	
		design after KPC review.	
0.15	10/5/05	Edited 201572 55 (pkg drwg) and	
		added the M08A mktg outline.	
0.20	11/01/05	Mjor edits on the EC table (by	
		Heather).	
0.25	02/02/06	Input major text (Typical limits)	
		edits.	
0.30	05/31/06	Some text edits.	
0.35	06/07/06	Edited Typical values on Zin.	
0.40	08/02/06	Added the Typ. Perf. Curves and	
		some text edits.	
0.45	08/07/06	Added the 2 curves	
		(Voltage/Current Noise Density vs	
		Freq.)	
0.50	08/08/06	Replaced some of the curves.	
0.55	08/10/06	Added more curves.	
0.56	08/16/06	Initial WEB.	
0.57	08/22/06	Changed the Typical values on	
		Instantaneous Short Circuit Current	
		from +30/-38 into +53/-42 (per	
		Robin S.), then re-released the D/S	
		to the WEB.	

#### Physical Dimensions inches (millimeters) unless otherwise noted В 6 ± 0 . 2 [ . 236 ± . 008] 6X (1.27 [.05] RECOMMENDED LAND PATTERN 1.35-1.75 [.053-.069] TYP R0.18±0.02 [.007±.0008] 6X [1.27 [.050] 45°X 0.25-0.50 [.010-.020] 0.1[.004] C 0.10-0.25 [.004-.010] TYP 0.41-1.27 CONTROLLING DIMENSION IS MILLIMETER VALUES IN [ ] ARE INCHES DIMENSIONS IN ( ) FOR REFERENCE ONLY M08A (Rev K) Narrow SOIC Package Order Number LM4562MA **NS Package Number M08A** $\frac{0.373 - 0.400}{(9.474 - 10.16)}$ 0.090 (2.286) 8 7 6 5 8 7 $\boldsymbol{0.032 \pm 0.005}$ 0.092 (2.337) $(0.813 \pm 0.127)$ $0.250 \pm 0.005$ PIN NO. 1 IDENT $(6.35 \pm 0.127)$ PIN NO. 1 IDENT OPTION 1 1 2 3 4 0.280 MIN <u>0.040</u> (1.016) 0.030 MAX (7.112) OPTION 2 0.039 0.145 - 0.200 0.300 - 0.320(0.762)(0.991)(3.683 - 5.080)(7.62 - 8.128) $0.130 \pm 0.005$ $(3.302 \pm 0.127)$ 0.125 - 0.140(3.175 - 3.556)0.065 0.020 0.125 (1.651) 0.009 - 0.01590°±4° (0.508) MIN (3.175) (0.229 - 0.381) $0.018 \pm 0.003$ $0.325 \, {}^{+\, 0.040}_{-\, 0.015}$ NOM $\overline{(0.457 \pm 0.076)}$ $0.100 \pm 0.010$ $(2.540 \pm 0.254)$ $0.045 \pm 0.015$ $(1.143 \pm 0.381)$ 0.060 (1.524)0.050 (1.270) N08E (REV F) **Dual-In-Line Package** Order Number LM4562NA **NS Package Number N08E**

### Physical Dimensions inches (millimeters) unless otherwise noted (Continued)



TO-99 Metal Can Package Order Number LM4562HA NS Package Number H08C

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